

## WARNING :

Attempting to change the value of some components during a simulation will not interrupt the execution but its outcome may become *silently misleading*

*Depending on the topology of the circuit*, some *flux* and/or *charge* may have to be partially redistributed on some other components

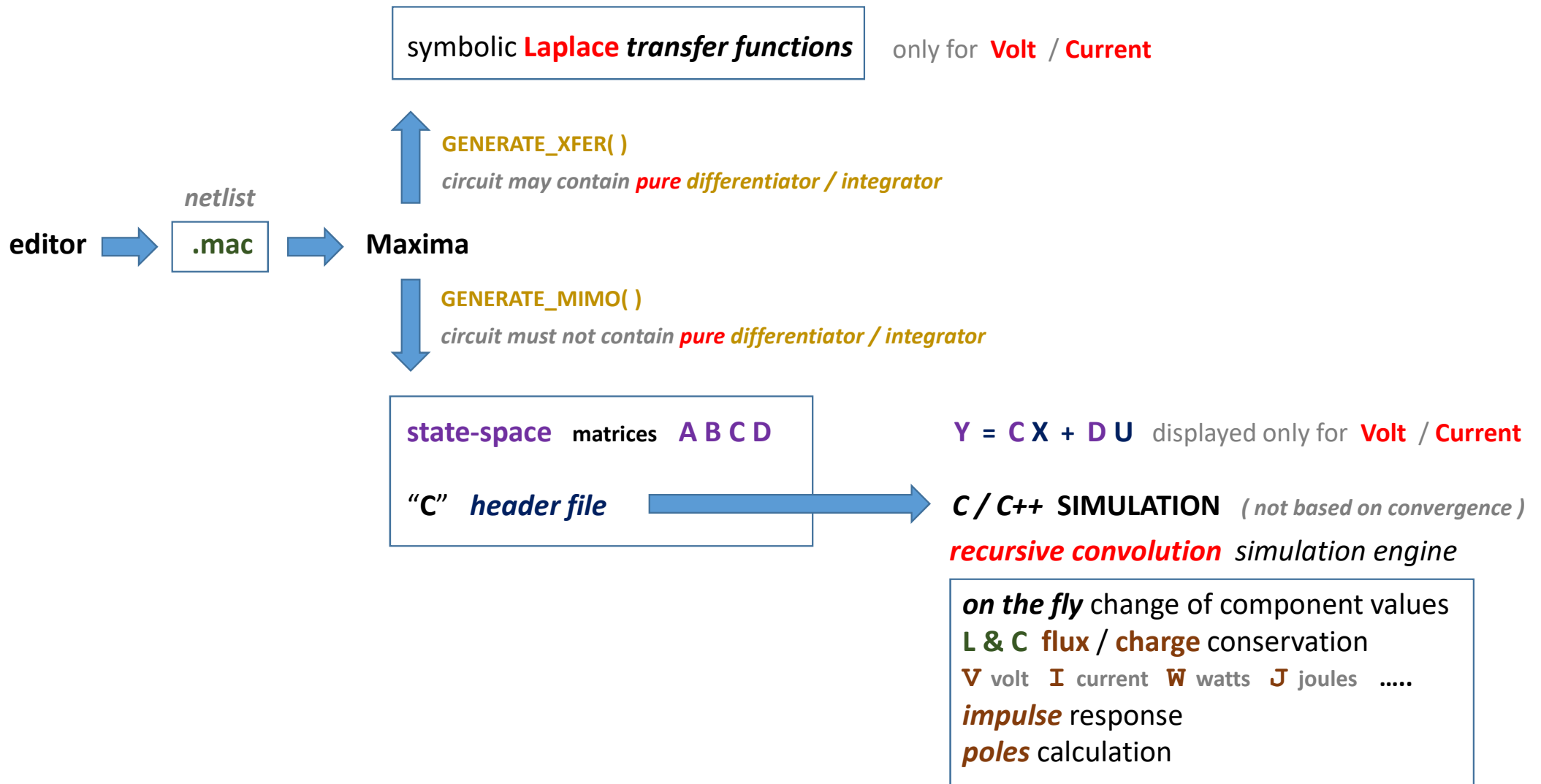
( trivial example : *changing the value of a capacitor in parallel with another one* )

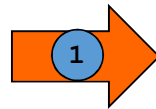
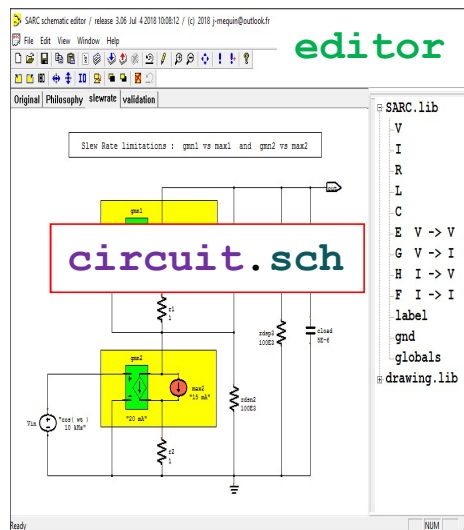
Therefore, simulating accurately component "*percussions*" requires some additional analysis, equations and processing

For *Laplace transfer function* (**XFER / ILT**) and *Z transform* (**ZTRANS**) such functionality has not been implemented and simulations may turn to be *silently misleading*

**In summary,**

only *STATE model* (**MIMO**) is able to simulate accurately "*on the fly*" component changes





netlist

```

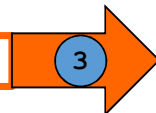
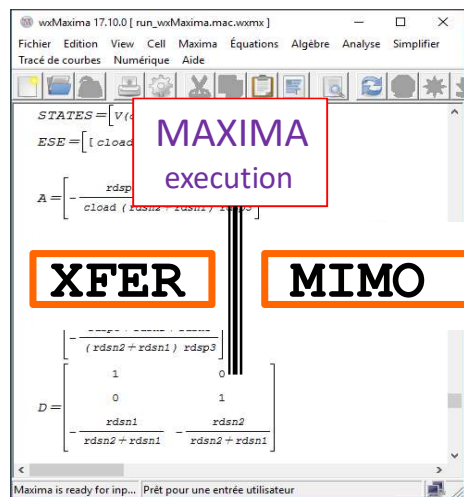
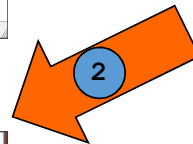
xmldocument : "slewrates"
xmllpage : "slewrates"
xmldate : "Fri Jul 6 11:07:33 2018 generated with release 3.06" ;

SCHEMATIC( "
Slew Rate limitations : gmn1 vs max1 and gmn2 vs max2
" ) ;

NETLIST(
[ I , max2 , n03 , n04 ] ,
[ R , r1 , n02 , n03 ] ,
[ R , r2 , n04 , GND ] ,
[ R , rdsn1 , out , n03 ] ,
[ R , rdsn2 , n03 , GND ] ,
[ R , rdsp3 , out , GND ] ,
[ C , cload , out , GND ] ,
[ G , gmn1 , out , n02 , GND , n03 ] ,
[ G , gmn2 , n03 , n04 , n01 , GND ]
) ;

```

circuit.mac



C headerfile

```

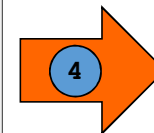
#define MIMO slewrates A { \
((-1.0e+9*Z[0])-210000.0)/(5.0e+8*Z[0]+55000.0) \
}

#define MIMO slewrates B { \
(((1.0e+9*Z[0])-100000.0)*Z[1])/(5000.0*Z[0]+0.55) , \
(((1.0e+9*Z[0])-100000.0)*Z[3]-10000.0*Z[2])/(5000.0*Z[0]+0.55) \
}

#define MIMO slewrates C { \
0.0 , \
((-1.0e+9*Z[0])-210000.0)/(1.0e+14*Z[0]+1.1e+10) , \
-100000.0/(1.0e+9*Z[0]+110000.0) , \
0.0 , \
-100000.0*Z[0]/(1.0e+9*Z[0]+110000.0) , \
0.0 \
}

```

circuit\_mimo.hdr



NAPA

A **schematic XML** file is called a “**DOCUMENT**” that can be

displayed on a resizable window

that may contain several “**PAGES**”

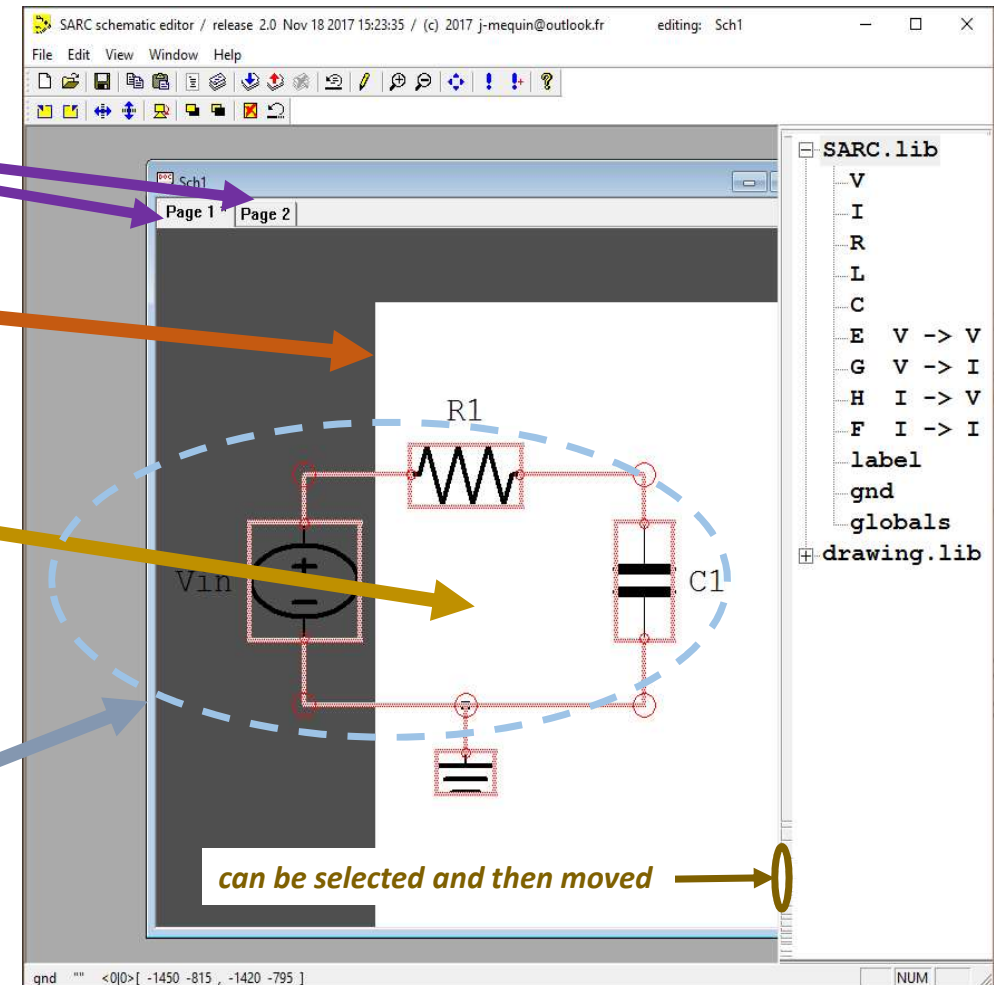
Each “**PAGE**” is a “**container**”

including the

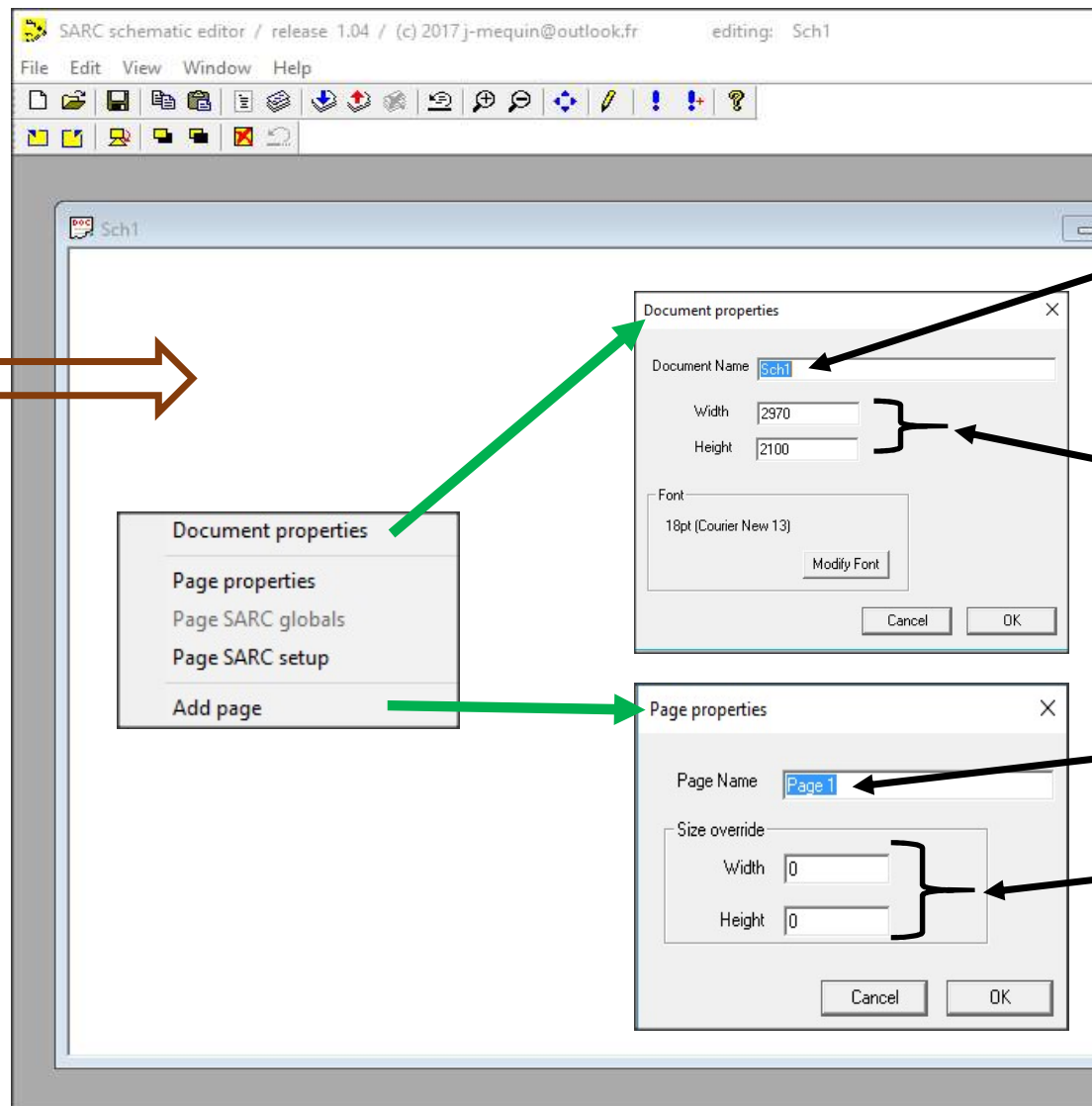
*available surface for the drawing*

by default **width** = 2970 **height** = 2100  
( thus *landscape* )

*this whole schematic needs to be moved to the printable area*



*click right*  
on an empty zone



document **name**  
will remain coherent with  
the XML and MAC **filenames**

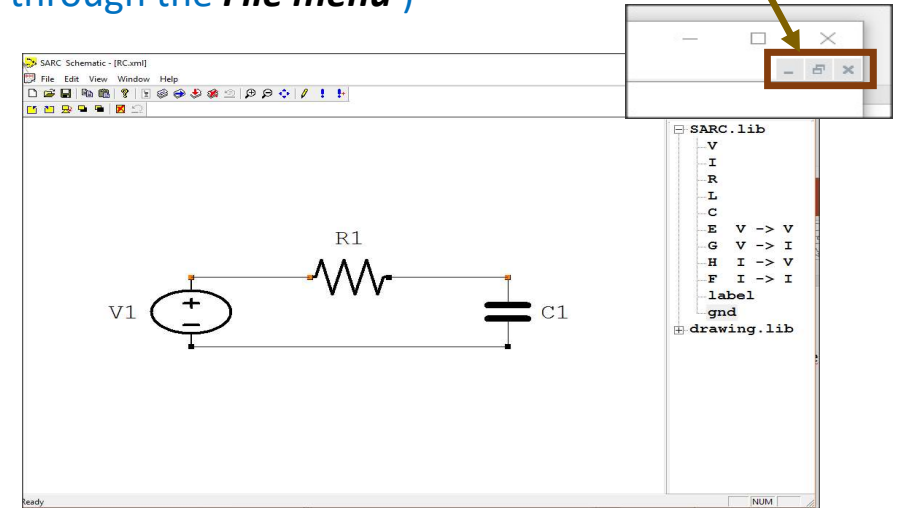
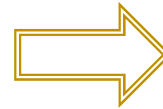
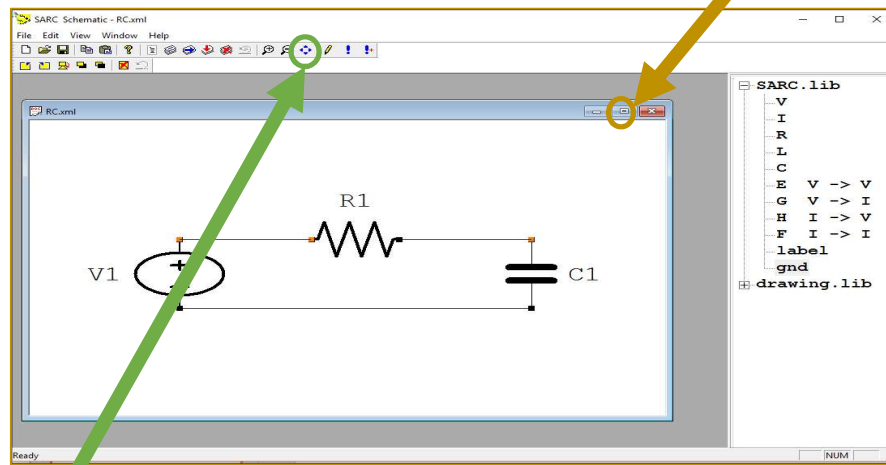
**width** and **height**  
of the default **printable area**

page **name**

**width** and **height**  
of this **page area**  
( 0 means same as document )

Several **XML** files can be active at the same time, allowing to **cut / paste** selected item(s) between them

A **single page** can be expanded to the full area by **clicking** ( and then , can still be **minimized** , **restored** , **closed** or **closed** through the **File menu** )



The  icon allows to **rescale** the schematic in order to fulfill the visible window area ( = ZOOM to fit )

**After positioning** the mouse, the **space bar** **centers** the view **without modifying the scale**

**After positioning** the mouse, **Page UP** increases the zoom by **25%**, **Page Down** decreases the zoom by **1/25%**, **around the mouse**  
or **Ctrl +** or **Ctrl -**

The **mouse wheel** can be also used to control the zoom

Any object on the “ Page ” can be selected by clicking left on it

Once selected, the objects can be

<i>copied</i>	<i>deleted</i>	<i>pasted</i>	<i>moved</i>
<i>ctrl-C</i>	<i>del key or ctrl-X</i>	<i>ctrl-V</i>	<i>click left</i>

Objects can be *deselected* by clicking on an *empty area* or with the *ESCAPE* key

Holding **Ctrl** key allows to select *all the objects* that are inside a *rectangular zone* delimited with the mouse *clicking left*

Once selected, the *area* can be

<i>copied</i>	<i>deleted</i>	<i>pasted</i>	<i>moved</i>
<i>ctrl-C</i>	<i>del key or ctrl-X</i>	<i>ctrl-V</i>	holding <i>ctrl</i> key + <i>click left</i>

An *area* can be *deselected* by clicking *elsewhere* or with the *ESCAPE* key

Holding **both Ctrl** and **Alt**, and then moving the mouse *clicked left* , allows to move **EVERYTHING** within the *page container*

*ctrl-Z*   **undo**   undo last edit operation(s)         **undo** icon

*ctrl-A*   **select**   *everything* on the *page*

**F2**   check page for missing connection diagnostics

*ctrl-C*   **copy**   whatever is *selected* to the clipboard

**F3**   display net names ( after netlist generation )

*ctrl-V*   **paste**   the contents of the clipboard

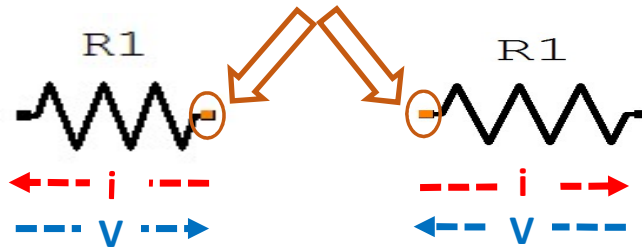
**F4**   playback all LIFO stack undo items

*ctrl-F*   **search**   an *instance name* ( or a NET name ) in the schematic





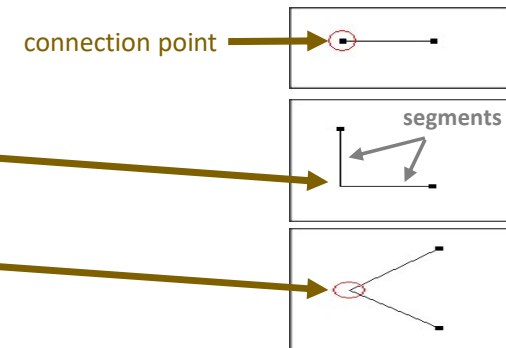
On each **SARC component**, an **orange mark** allows to identify, *despite possible rotations*, its **SARC netlist pins order**



Holding **Alt** key while **clicking mouse left** allows to **draw a WIRE segment**

While holding the **Alt** key, **toggling the mouse left** allows to **change direction**

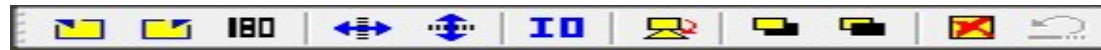
Without holding the **Alt** key, **clicking the mouse left** allows to **drag the selected location** of an existing **WIRE**



Pressing **F1** allows to make disappear **BOTH** the **orange marks** and the **connection points** ( *example, for nicer plot* )

The **SARC component "label"**  can be used to associate a **name** to a **NET** ( *overriding its default "nxx"* )  
*"Distant labels" sharing same name are wirelessly connected !!!*

The objects **"Title"** or **"Sticker"** of the **"drawing.lib"** can be used to add some **legends** to the schematic

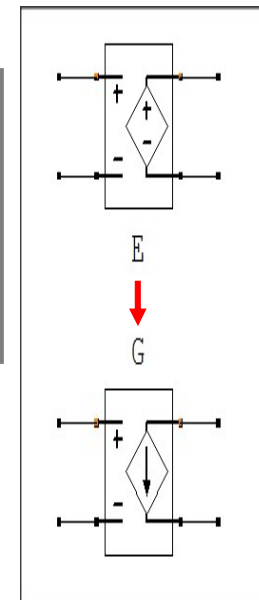
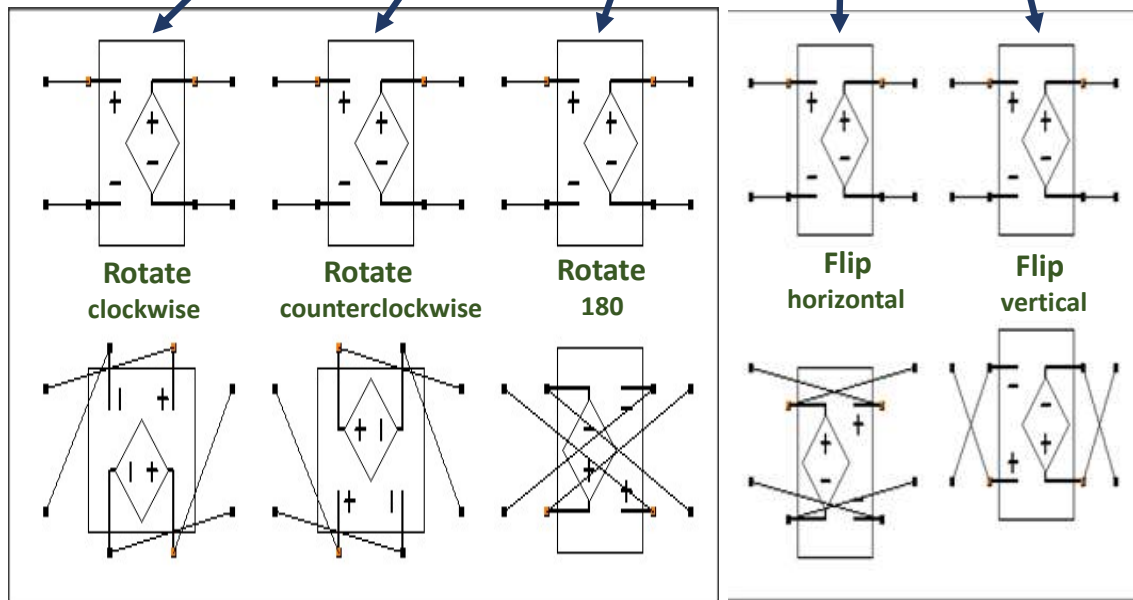


“undo” previous edit / ctrl-Z  
from the *history* queue

delete **selected** object(s) / ctrl-X

change  
component **type**

I/O swap can be used  
to reverse **V I R L C**  
and **only** outputs of  
**E H G F**



← connected nets remain attached →

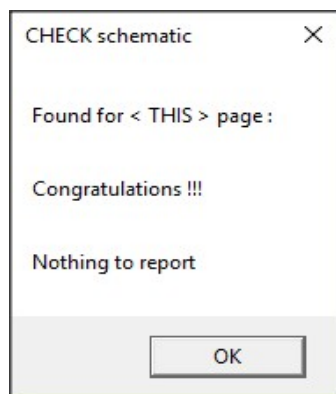
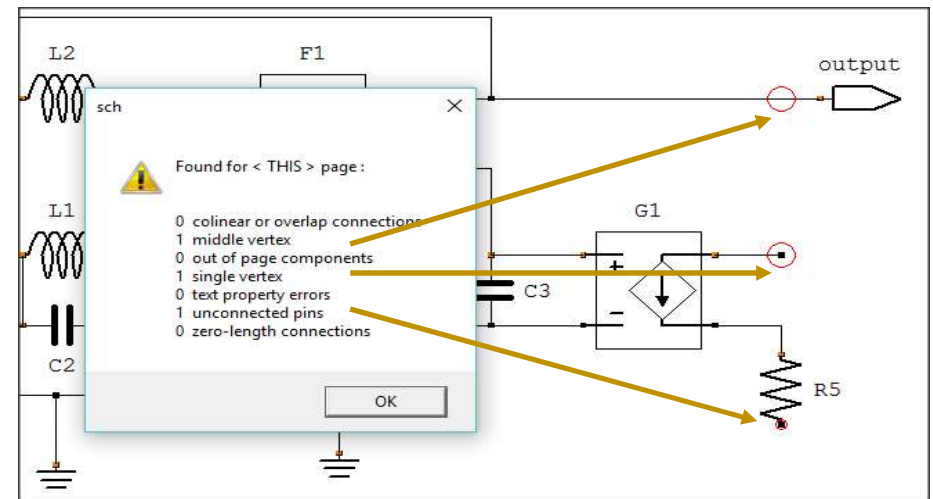
Before the *netlist generation* it is **mandatory** to perform some **sanity checks** on the schematic(s)

Those checks are **almost the ones of the original software** and are **not as exhaustive as** the *SARC Maxima* version

**Therefore**, even if a netlist is later generated, it can still contains some remaining issues

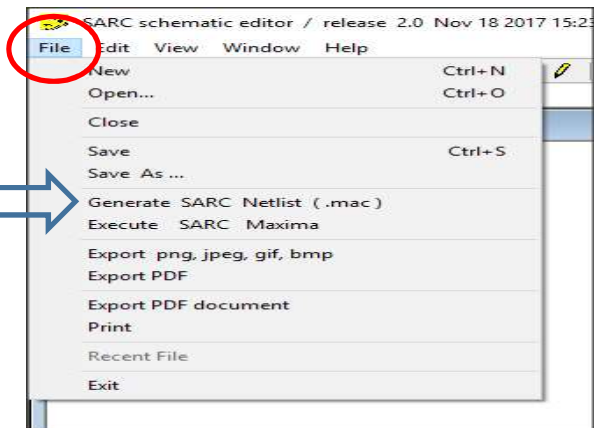


**On the current page**, it is also possible to display the **diagnostics** of the checks, **but without the pop-up window**, by pressing **F2**



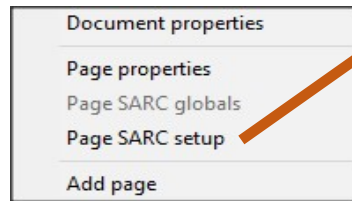
Netlist generation  
same *file location* that  
the associated **XML**

File menu



Maxima SARC parameters can be  
*collected* and *saved* within the XML

However, this release *does not yet check* them



SARC setup

INTERN Offs

OUTPUTS V( Out ) , I( Rload )

close window  
or *Escape* key

execution order 2

GENERATE\_XFER ☒ nointern

execution order 1

GENERATE\_MIMO

showxfer ☒

XWISH L1 , C1 , C2

generate XFER or MIMO with/without display

can be only modified when MIMO *execution order*  $\neq 0$

separator ,

```
limit ( XFER[1] , A , inf ) ;
```

User code  
Maxima

execution order

2

1

GENERATE\_MIMO ( )

GENERATE\_XFER ( )

can be only modified when XFER *execution order*  $\neq 0$

special  
control  
directives ☐

Cancel

OK

document property "**name**"

( that is related to *filename* )

page property "**name**"

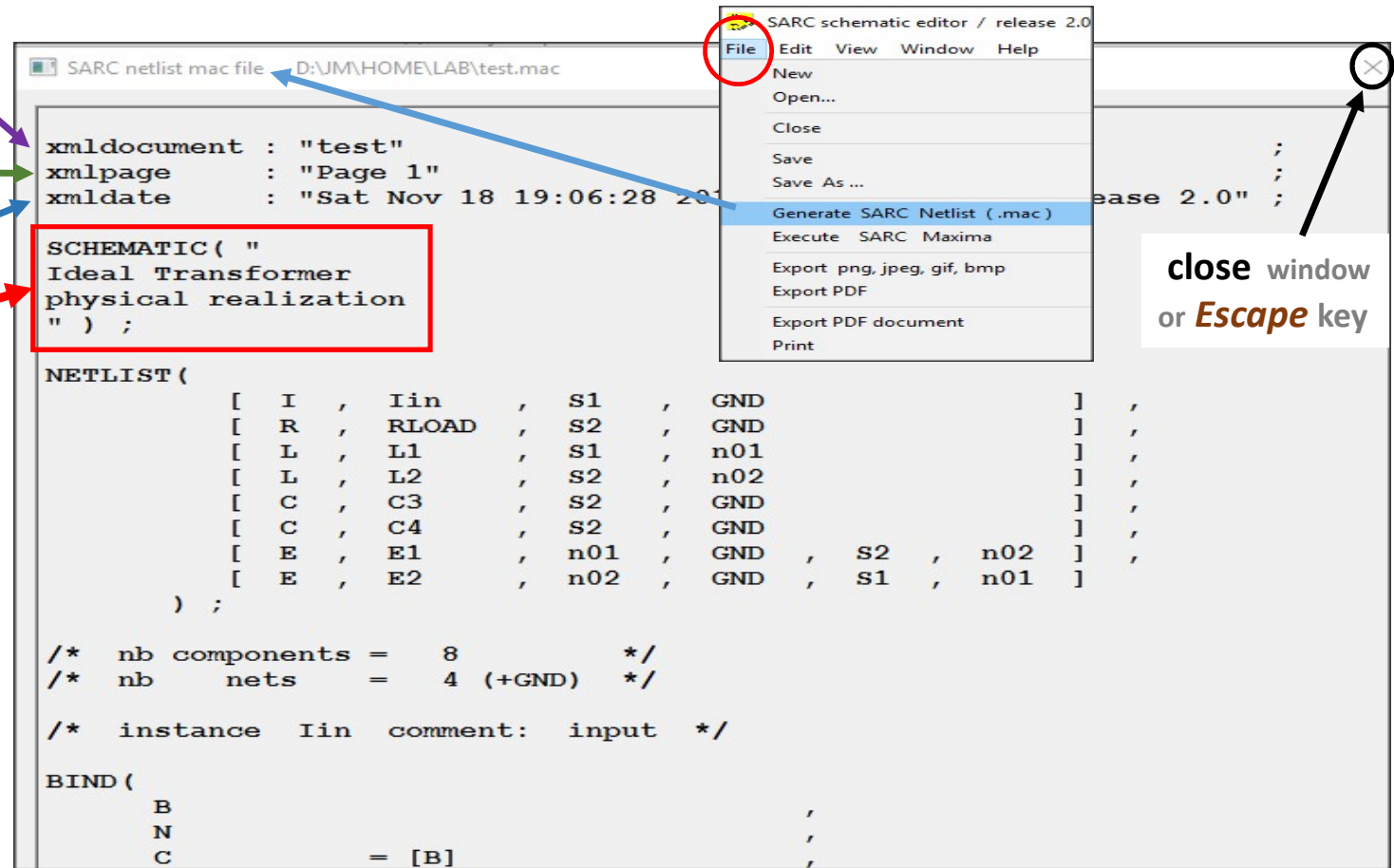
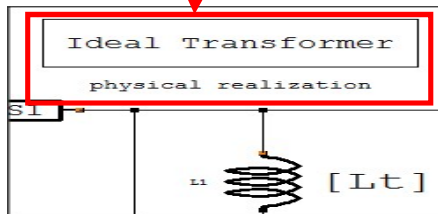
generation date

when defined ,  
those lines come from

**drawing.lib**

"**Title**" objects

"**Component additional legends**"



close window  
or **Escape** key

In case of several **Title** use « **Bring to front** » icon to select one of them

**Escape-S** can be used to view the **current** schematic **".sch"** file

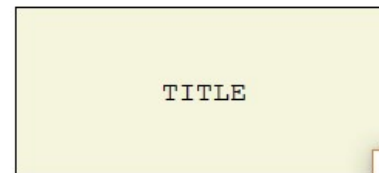
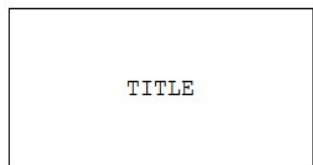
**Escape-P** can be used to view ( **AFTER schematic Save / Save as** ) the **latest** generated **".pdf"** file

**Escape-M** can be used to view ( **AFTER generate SARC Netlist** ) the **latest** generated **".mac"** file

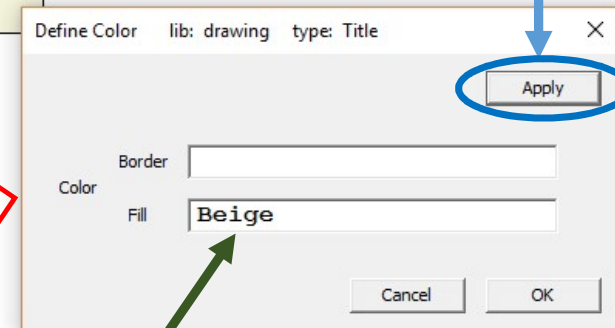
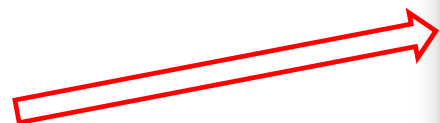
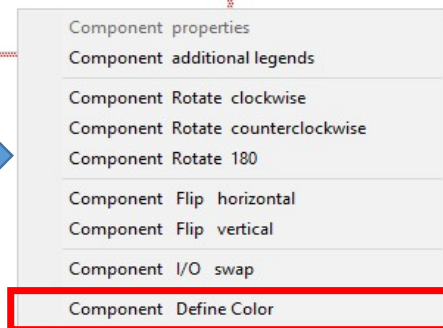
**Escape-H** can be used to view ( **AFTER GENERATE\_MIMO( )** ) the **latest** generated **".hdr"** file

**Escape-Z** can be used to view ( **AFTER GENERATE\_Z( )** ) the **latest** generated **".hdr"** file

**Escape-C** can be used to view the **colormap**



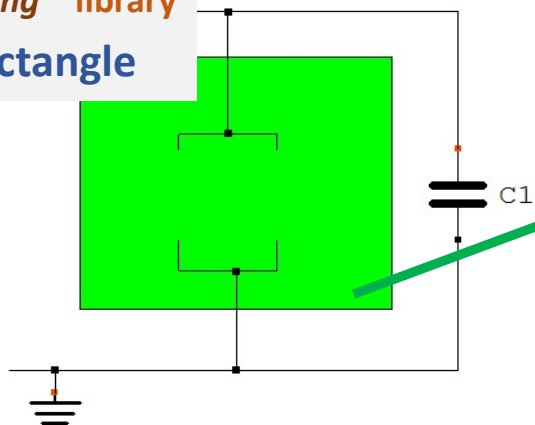
right click



test effects but keep popup

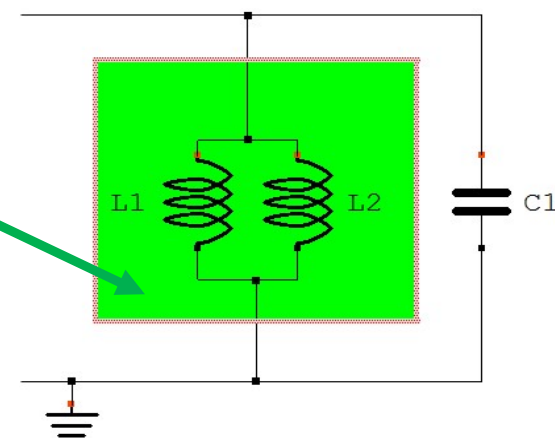
define in file *colormap* (*Escape-C*)

*"drawing" library*  
Rectangle

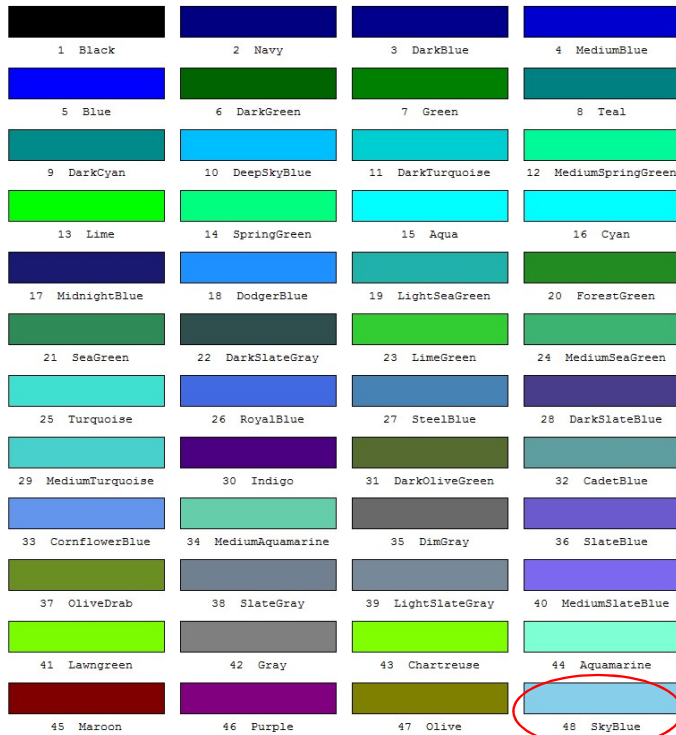


Bring  
to Front

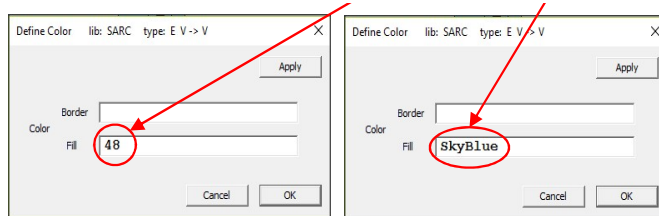
Bring  
to Back







**COLORS** can be defined



by **index** or by **name** (*case insensitive*)



*ESC* - C





## OUTPUT syntax examples :

SARC setup

INTERN	<input type="text"/>
OUTPUTS	V( Cx ) , V( Cy ) , I( Rx ) , I( Ry )

**V**( *label* )

label : netlist node

**V**( *label1:label2* )

voltage between 2 labels ( note: GND is a label )

**V**( *component* )

components : U I R L C and E G H F outputs

**I**( *component* )

components : U I R L C and E G H F outputs

**W**( *component* )

components : U I R L C and E G H F outputs

**cV**( *voltage control* )

control side of E G

**cI**( *current control* )

control side of H F

...

note : the **Y[ ]** vector *displayed* by wxMAXIMA only contains **V( )** **cV( )** **I( )** **cI( )**

## component parameters

★ string « hello world » *comments are ignored by Maxima*

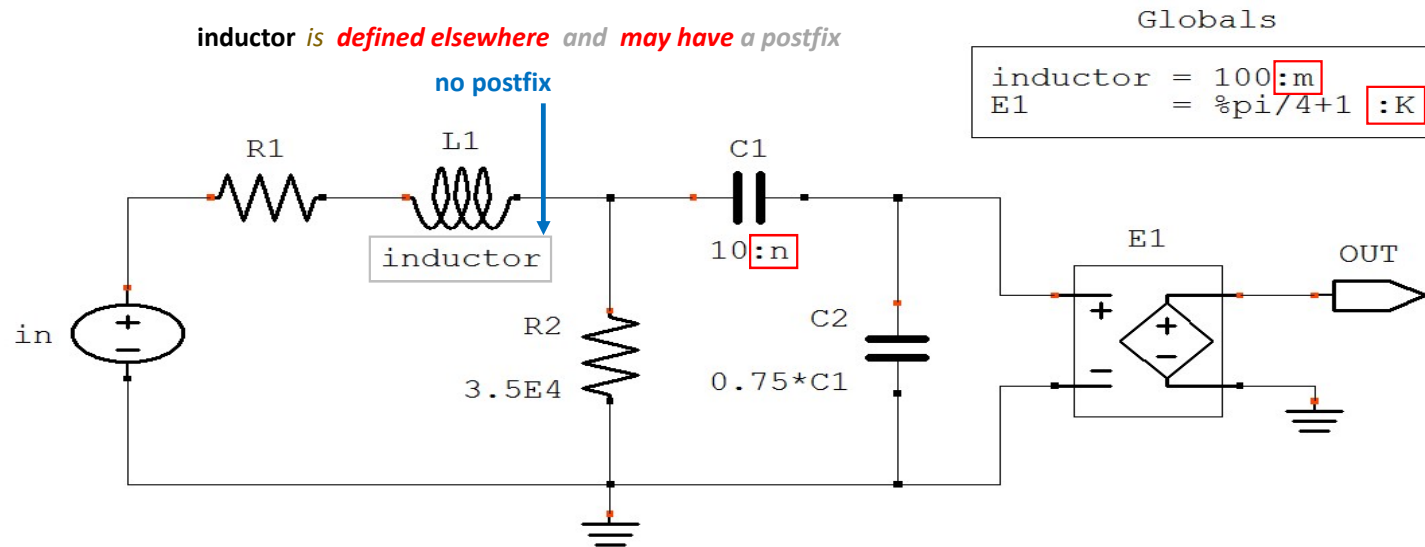
★ symbolic  $3*gain$   
 $k*\sqrt{gain}$   
 $0.8 / gain$

*substituted at the start of Maxima analysis*  
*symbolic definitions must reference at least one variable*

NOTE : *special syntax* [1] [+1] [-1] ( 1 is the only accepted « value » )

★ numeric 0.4  
12E-3  
 $\sqrt{\%pi}$

*substituted at the end of Maxima analysis*  
*numeric definitions must not reference any variable*



schematic instance *numeric values* can be *postfixed* with a multiplicative unit

:P	<i>peta</i>	$10^{+15}$
:T	<i>tera</i>	$10^{+12}$
:G	<i>giga</i>	$10^{+9}$
:M	<i>mega</i>	$10^{+6}$
:K	<i>kilo</i>	$10^{+3}$

*uppercase*

:m	<i>mili</i>	$10^{-3}$
:u	<i>micro</i>	$10^{-6}$
:n	<i>nano</i>	$10^{-9}$
:p	<i>pico</i>	$10^{-12}$
:f	<i>femto</i>	$10^{-15}$

*lowercase*

# Globals

A special SARC component named « **globals** » can be instantiated on the page

Its purpose is to define **circuit global parameters** referenced by **instance values** or other **globals**

user  
globals  
identifiers  
declaration

comment

numeric value

symbolic expression

Maxima VAR = EXPRESSION

K = "small"

C1 = 1E-9

K1 = PHI1 \* sqrt( k )

C2 = K \* C

After placing the **globals** component, the **global menu** can be accessed by **right click** on an **empty area** of the screen or **double click left** on the **globals** component

SARC globals lib: SARC type: globals

Title Globals

Maxima VAR = EXPRESSION

L0 = 1E-4

L1 1E-3

L2 L0 + L1

Globals

L0 = 1E-4

Component properties

instancename

instvalue

Component properties

instance NAME

C2

instance VALUE

a **numeric** can be

- a number 1E-3
- a rational  $\frac{1}{2}$
- a calculus  $1E-3 + \frac{1}{2} * \text{sqrt}(\%pi)$
- not referencing instname or global

comment numeric symbolic

"small" 1E-8 K \* C3

global or instname

the function **XFLOAT( expr )** can be used to replace all **F%nn** with their **numerical values**  
the function **XNUM( expr )** can be used to replace all **Globals** with their **numerical values**

**NOTE :** any **symbolic constant** value of the form [ 1234 ] are **not allowed** except [1] [+1] [-1] that are reserved for **E , H , G , F** components

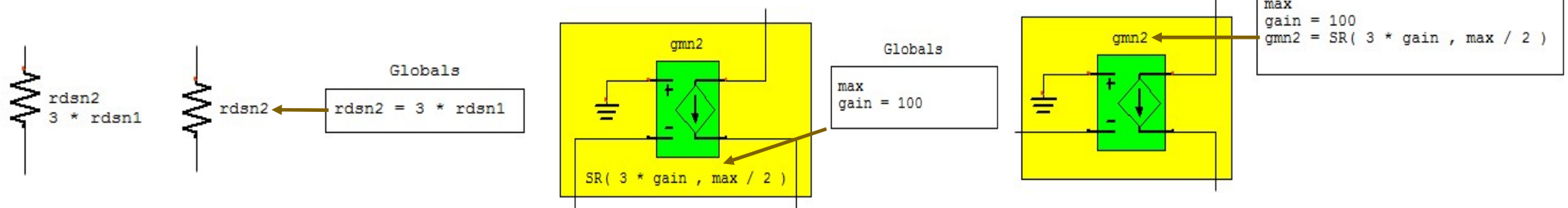
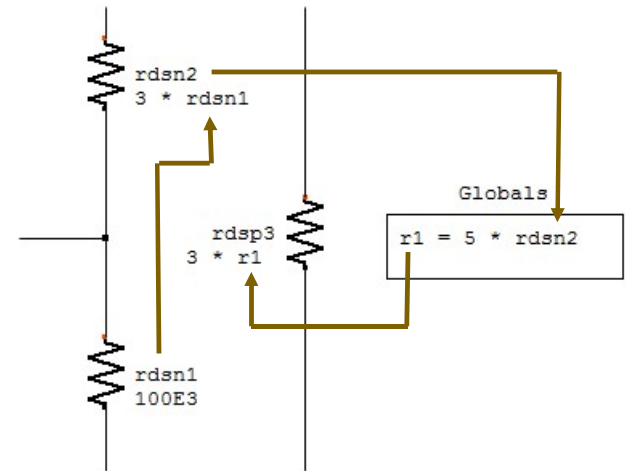
◆ **instnames** and **GLOBALS** variables can both be used in equations

◆ **instnames** are by definition « declared » and « used »

◆ **GLOBALS** variables must be also « declared » and « used » ( in **instvalues** or **GLOBALS** )

**R1**    **R1 = « load »**    **R1 = 100**    **R2 = 2 \* R1**

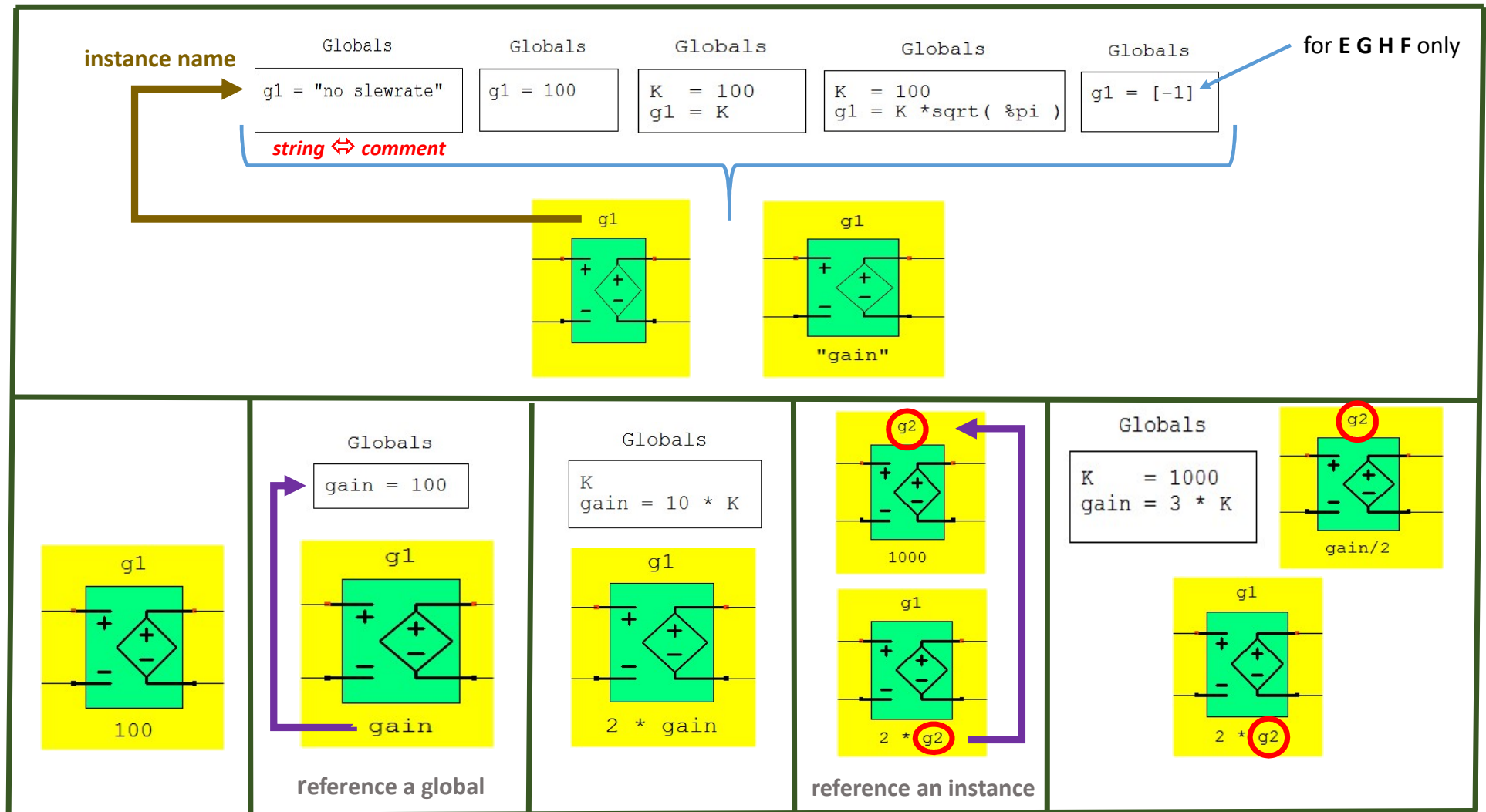
◆ equations can be defined either in **instvalues** or **GLOBALS**



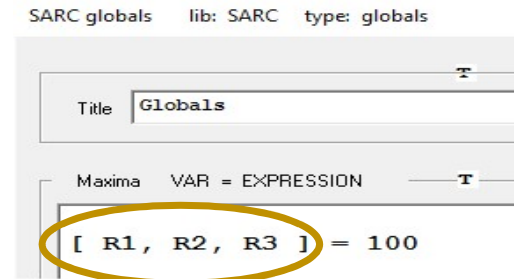
« XXX » **ignored string**

xxxx **symbolic** expressions substituted at **build time**

33.5 or 3E-8 **numeric** substituted at **run time**



declarations can be grouped



**runtime** directives can also be defined with **GLOBALS**

**%rubmode** = true

**%printpoles** = 3

**%srtol** = 1E-3

**%srlim** = 25

**%phases** = [ Phi1 , Phi2 ]

**%zopen** = Gds

**%zopen** = [ Gds1 , Gds2 ]

**%zshort** = Rds

**%zshort** = [ Rds1 , Rds2 ]

do not plot **instantaneous** percussion spikes ( simulation remains unchanged ) ( default false )

report the computations of the poles **due to the first 3 BOM** changes ( default 0 )

**saturation rendering** computation **tolerance** ( default 1E-4 )

roughly, dividing **%stol** by 10 increases the number of iterations by +4

**saturation rendering** computation **iteration limit** ( default 50 )

**mandatory** for **Z transform** but can be declared for **XFER / MIMO** ( no default )

component 'Gds' will be **ignored** by **GENERATE\_Z( )**

component 'Rds' will be **shorted** by **GENERATE\_Z( )**

In electronic, **slew rate** is defined as the *maximum change of **current** or **voltage** per unit of time* (  $\max(di/dt)$  or  $\max(dv/dt)$  )  
**but**, *rather than this « slope control »*, **SARC slew rate** simulates the **OP amp « clipping »** effect on **current** sources

In other words, for **G** and **F** `SR( gain , imax )`  $\leftrightarrow$  clipping **current** = **imax**

**gmn1** and **gmn2**

will both simulate

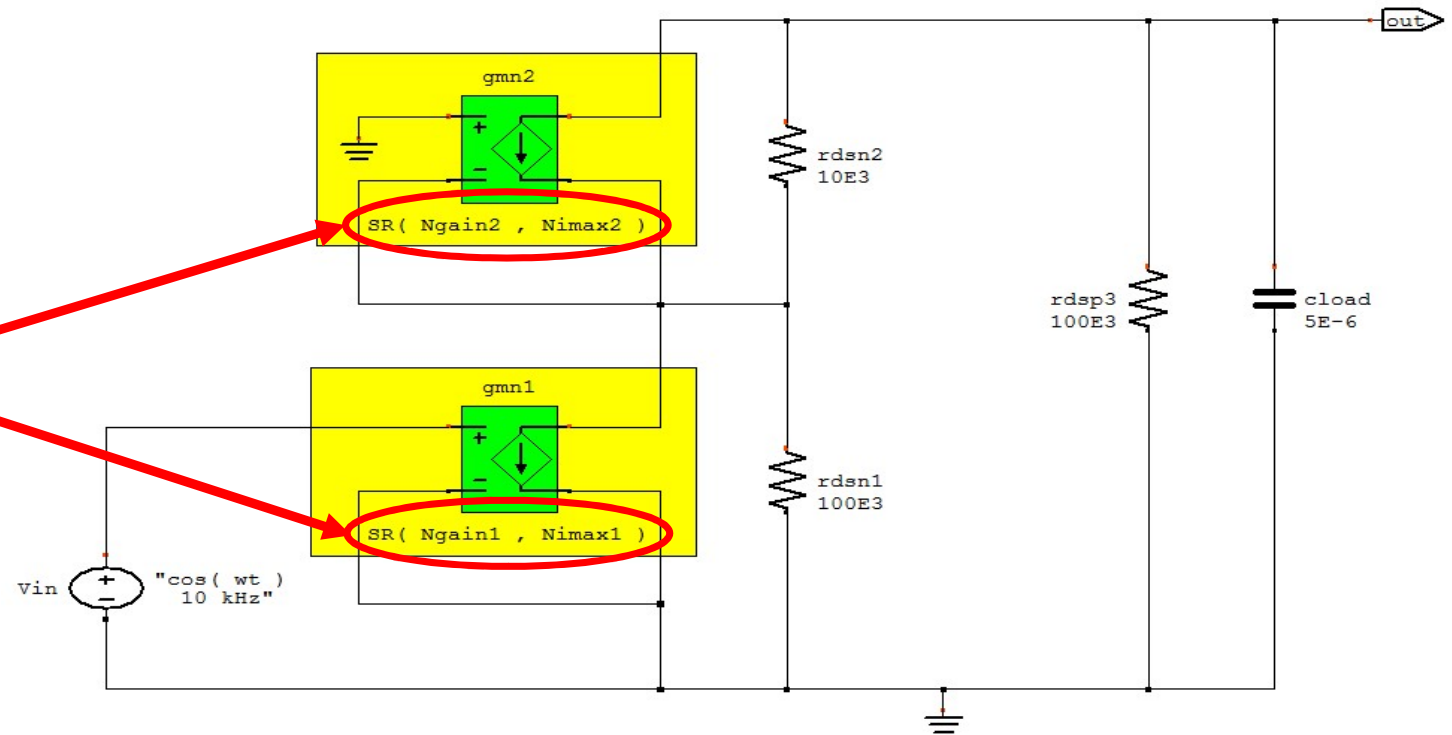
**Saturation Rendering**

« **OP amp SLEW RATE** »

Globals

```
%srtol = 1E-3
%srlim = 25
```

**targetted tolerance** = **fabs**( ( **maxOUTPUT** - **currentOUTPUT** ) / **maxOUTPUT** )  
**max iterations**





**Norton - Thévenin** previous slide

by duality,

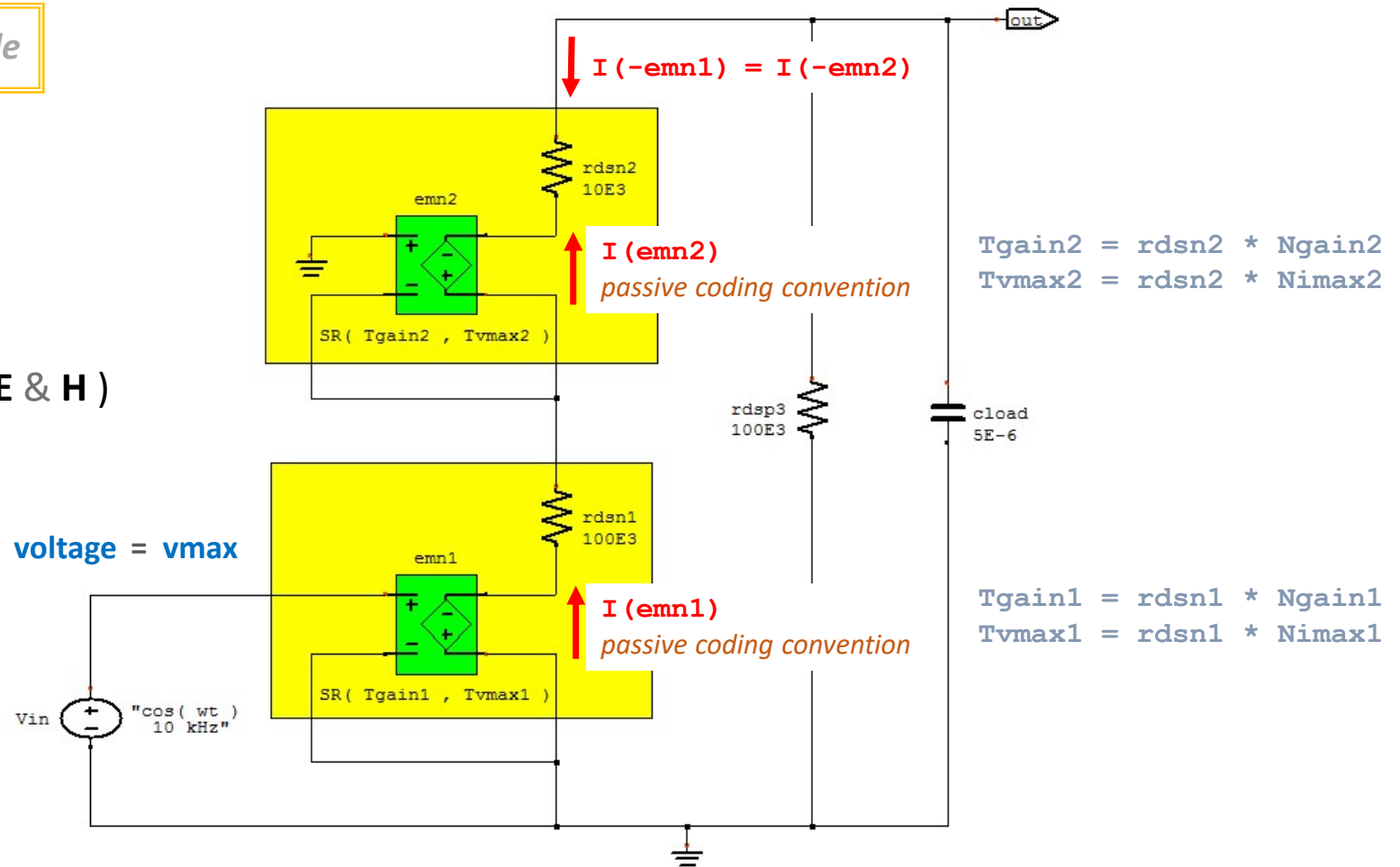
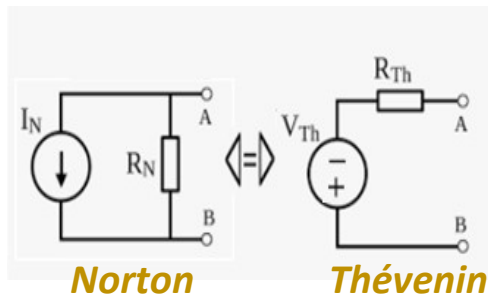
a similar « saturation effect »

can also be defined

for **controlled voltage source** ( E & H )

In other words, for E and H

$\text{SR}(\text{gain}, \text{vmax}) \iff \text{clipping voltage} = \text{vmax}$

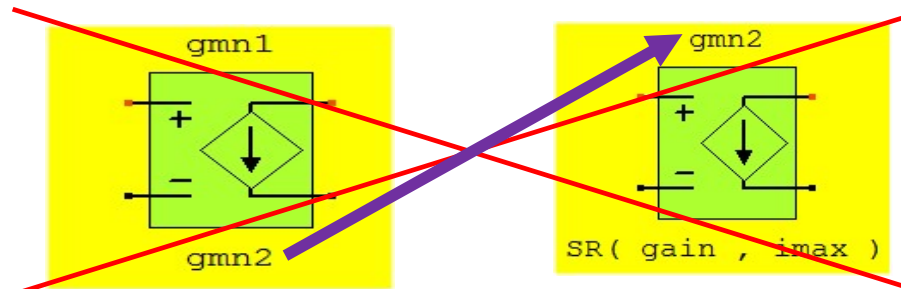
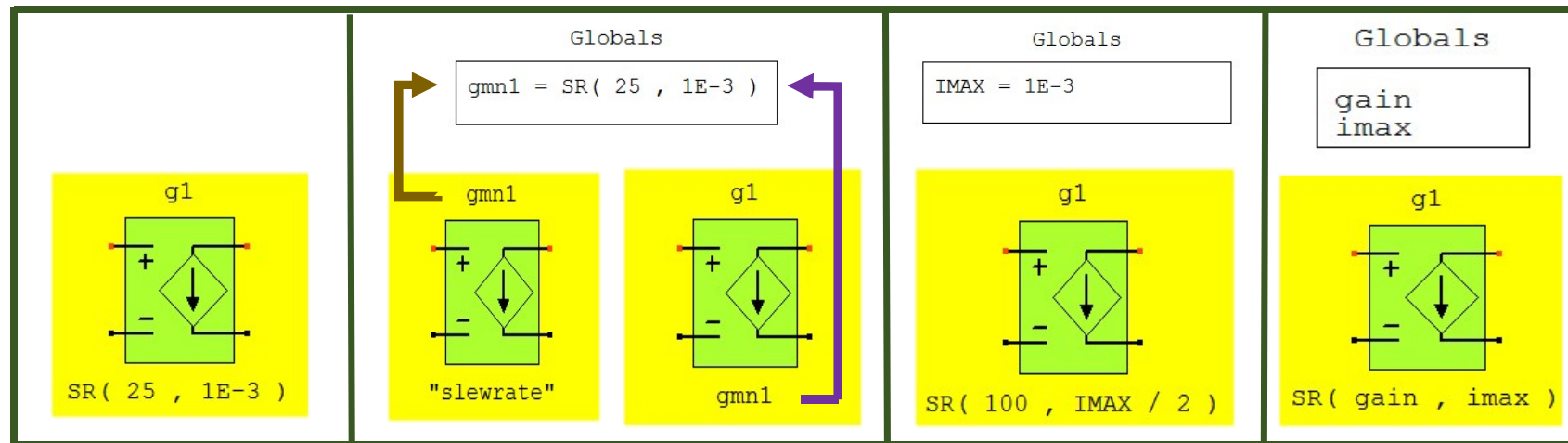


# SR( gain , maxout ) syntax

**maxout**    **Imax** for G and F  
               **Vmax** for E and H

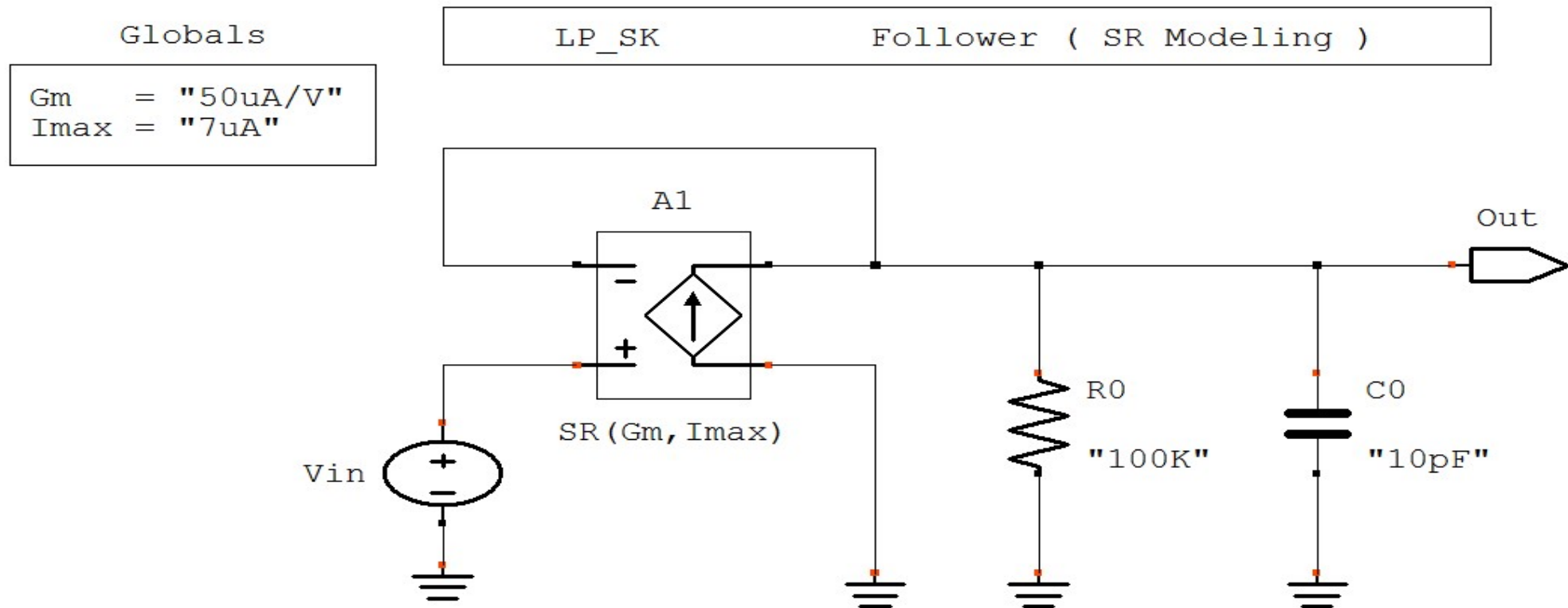
**maxout** = 0 → linear mode

**maxout** sign ignored



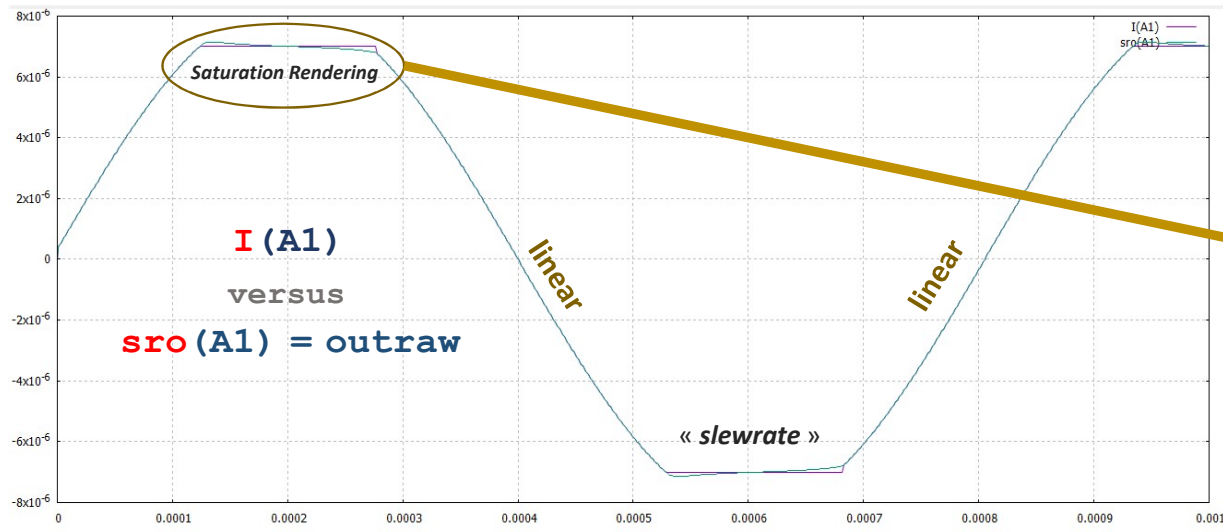
**gm1** gain cannot depend on **SR( )** of **gm2**

**There is no need to have several schematics :** **GENERATE\_XFER** and **GENERATE\_Z** ignore **SR( )** declarations  
**GENERATE\_XFER** and **GENERATE\_MIMO** ignore **%phases** declarations  
**MIMO SR( )** simulations can be performed **LINEAR** by setting **maxout** = 0

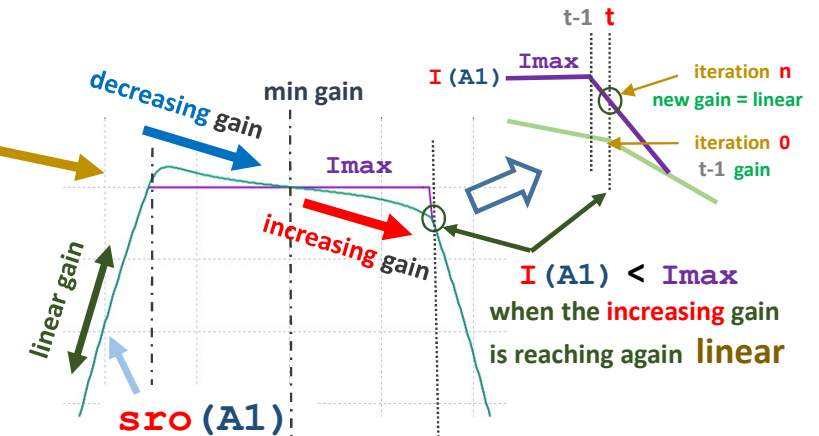


*3 special outputs can be plotted to observe the **Saturation Rendering** convergence*

- srn** ( A1 )    number of recalculations
- sro** ( A1 )    raw output before relaxation
- srg** ( A1 )    effective reduced gain necessary to sustain max output



# CONVERGENCE

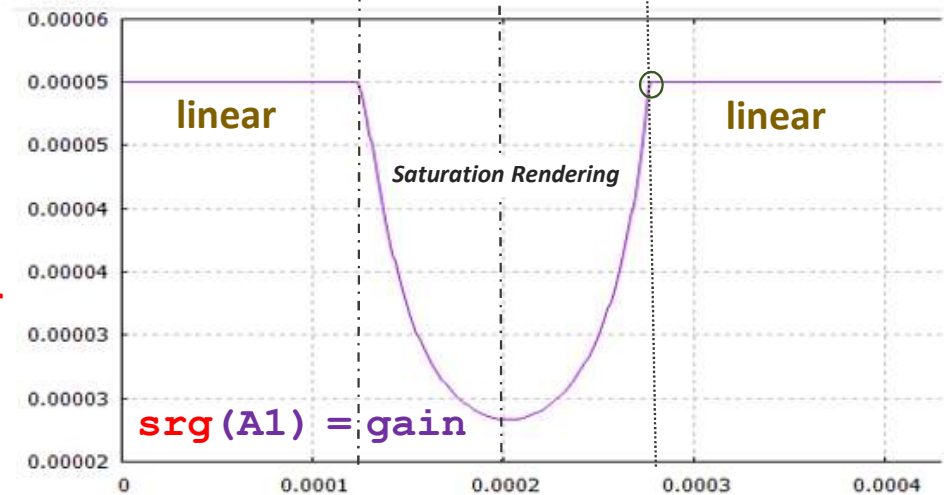


SARC is dedicated to **Linear Time Invariant** analog circuits

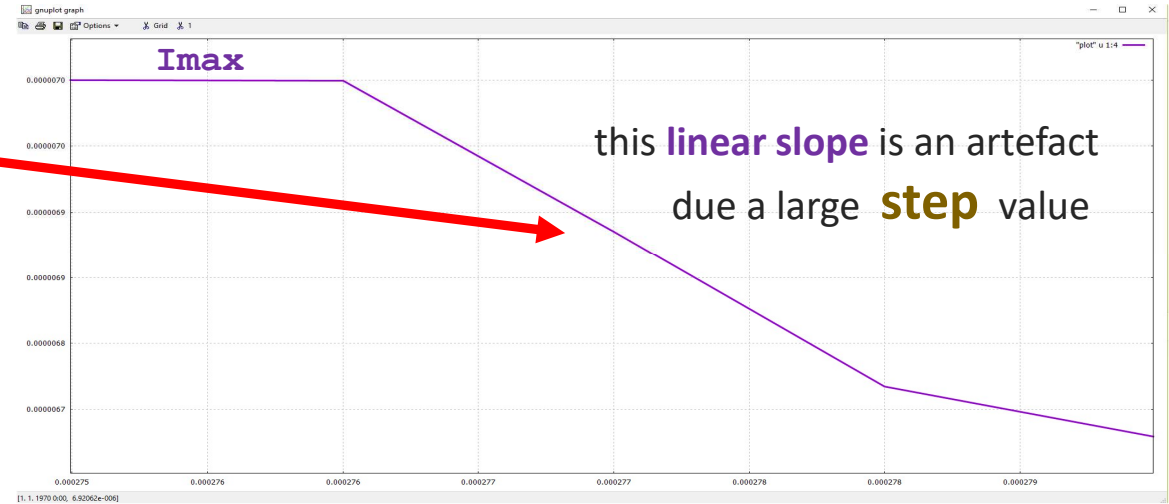
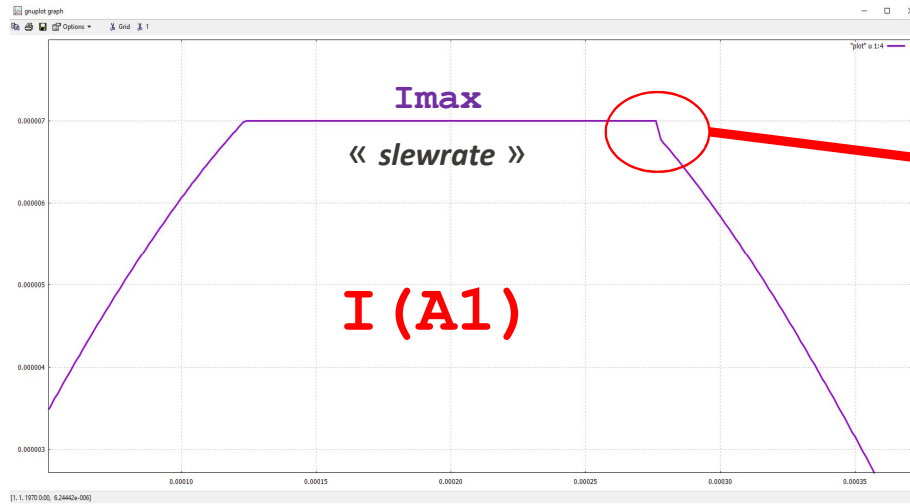
However,

SARC supports « **Saturation Rendering** » that is a **nonlinear behavior**

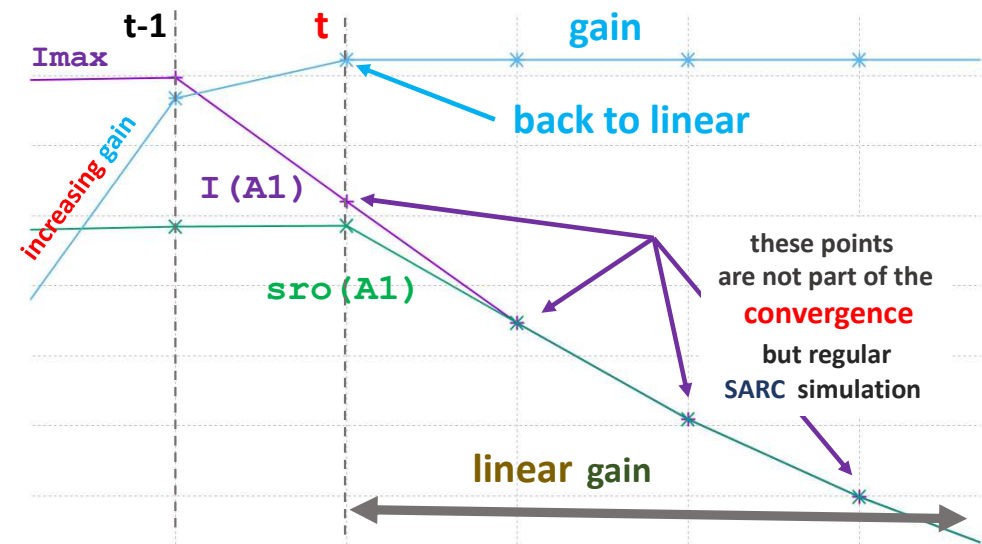
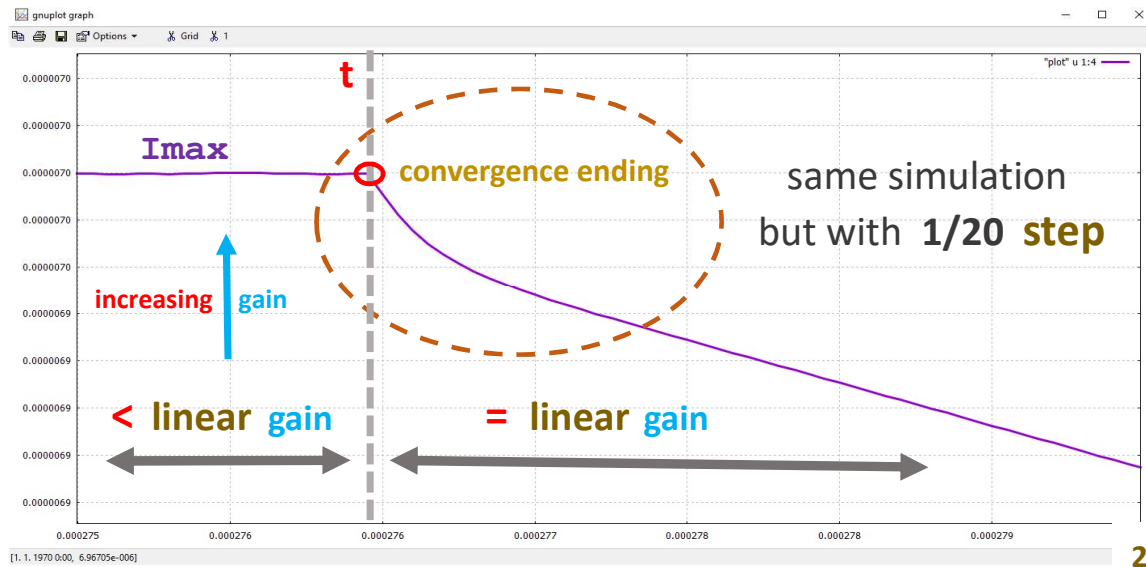
This can be only simulated through a **convergence process**

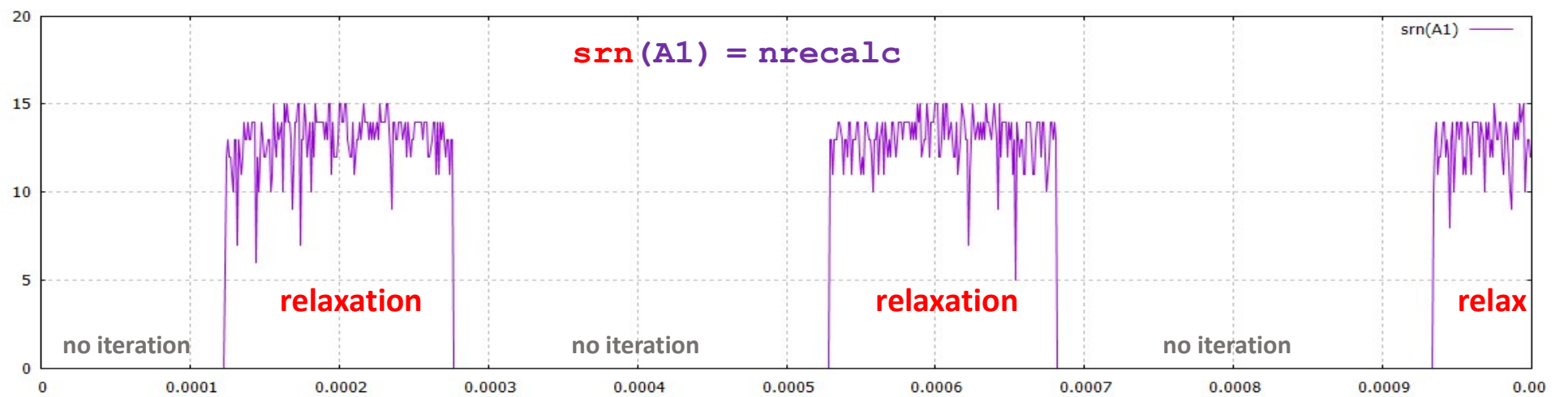
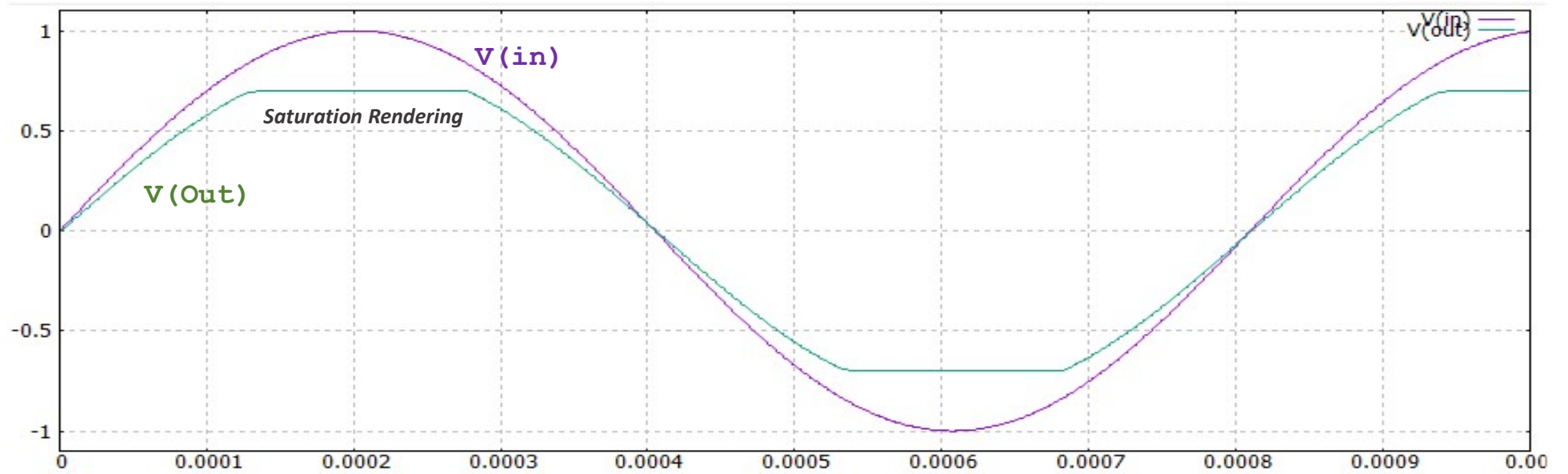


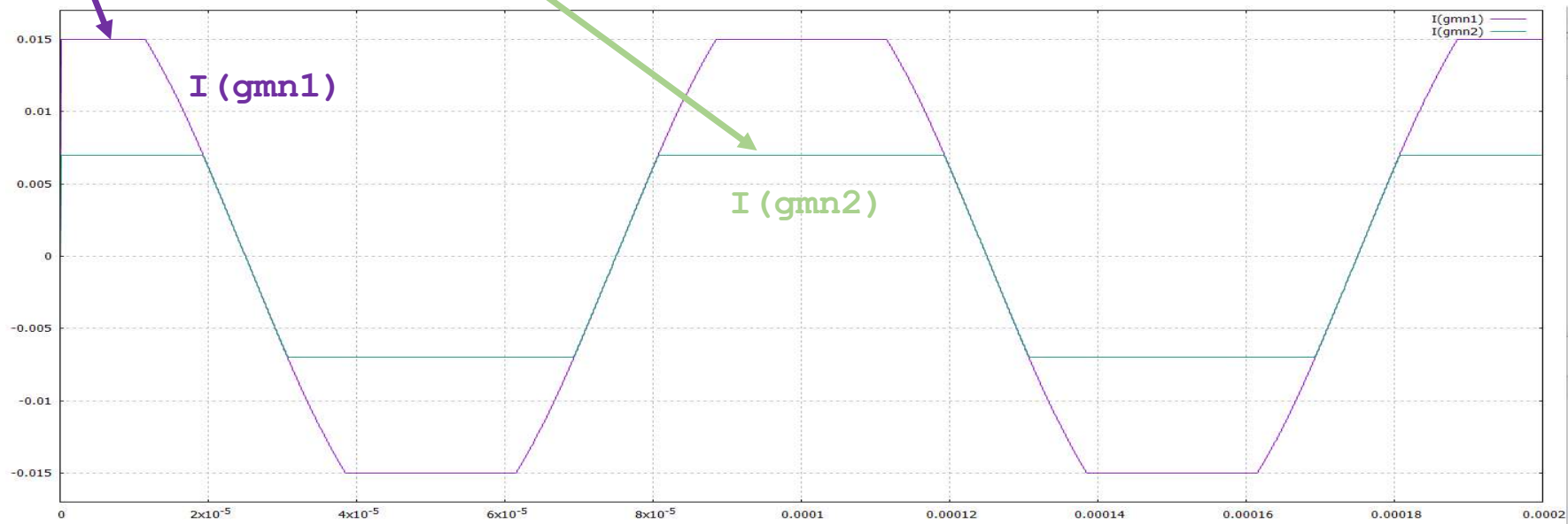
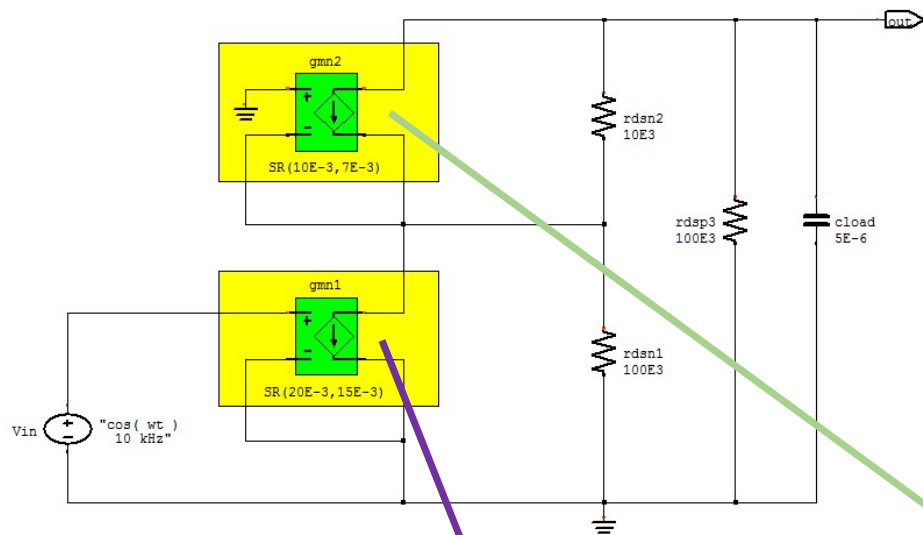
effective reduced gain necessary to sustain max output



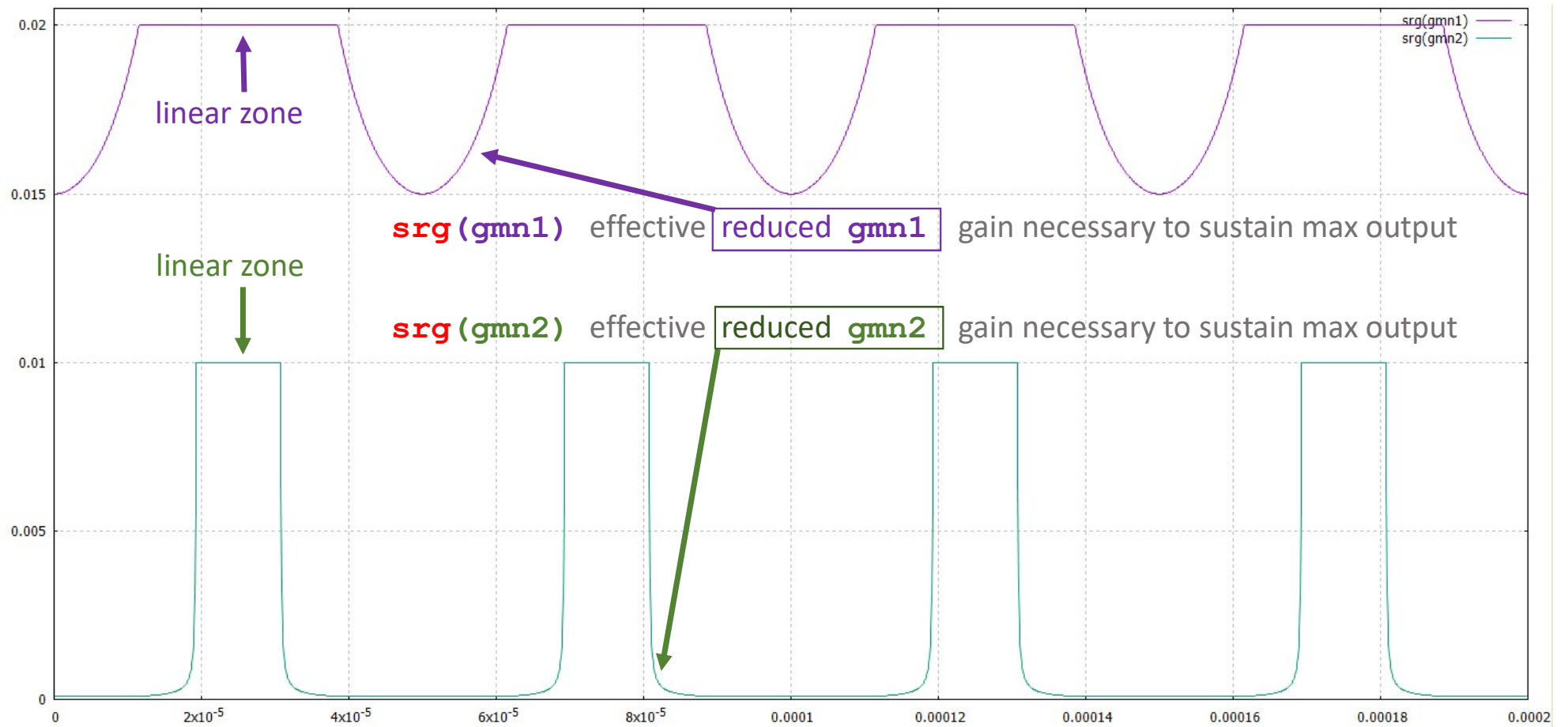
## CONVERGENCE ENDING





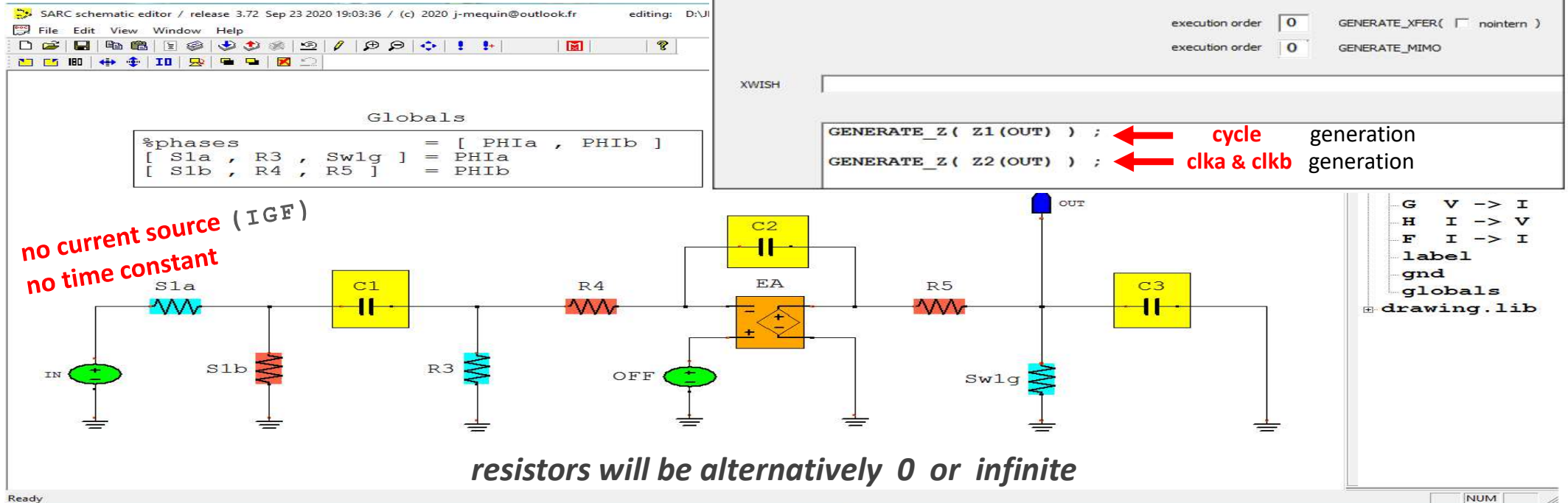








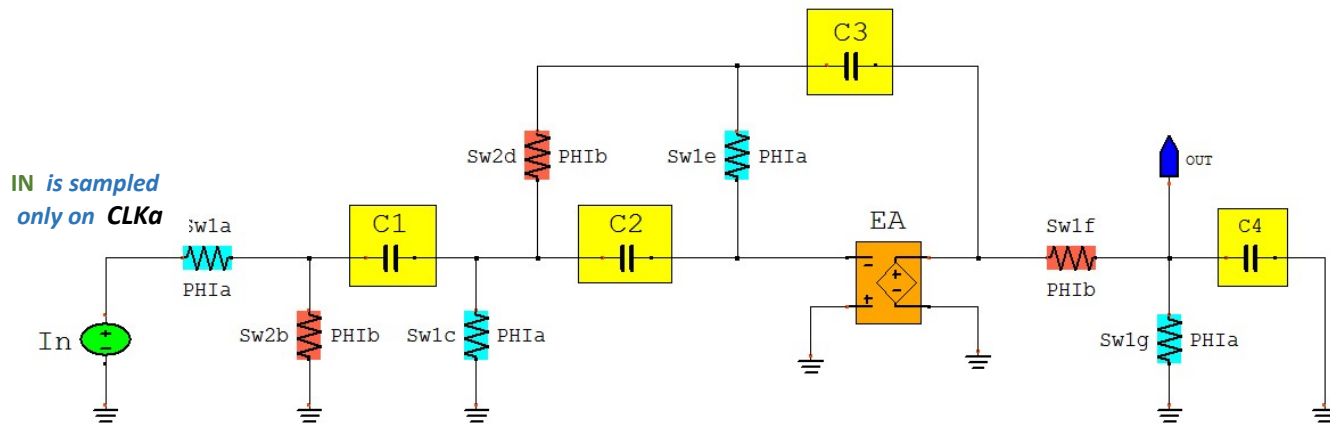
# Z transform



« **cycle mode** » means « **single sampling of the inputs per cycle** »

Therefore,

it only makes sense to request « **cycle model generation** » for **physical designs structurally insensitive to intracycle stimuli** ( **otherwise** this can also be achieved by **externally « latch » the inputs within cycle** )



... time response ( when CLKb )

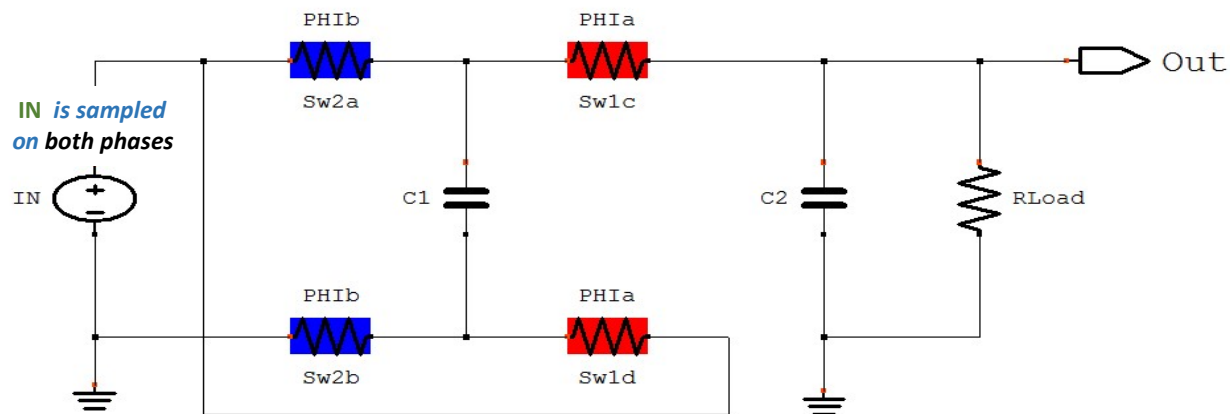
$$OUT_0 = \frac{nbIn_2 \boxed{In_{-1}} + nbIn_0 \boxed{In_{-3}} - db_1 OUT_{-2}}{db_3}$$

only odd indexes  
→ CLKa

... time response ( cycle )

$$OUT_0 = \frac{nIn_1 In_0 + nIn_0 In_{-1} - d_0 OUT_{-1}}{d_1}$$

== NOTE: CYCLE mode will remain exact even in case of intracycle INPUT changes



... time response ( when CLKb )

$$Out_0 = \frac{nbIN_1 IN_{-1} + nbIN_0 \boxed{IN_{-2}} - db_0 Out_{-2}}{db_2}$$

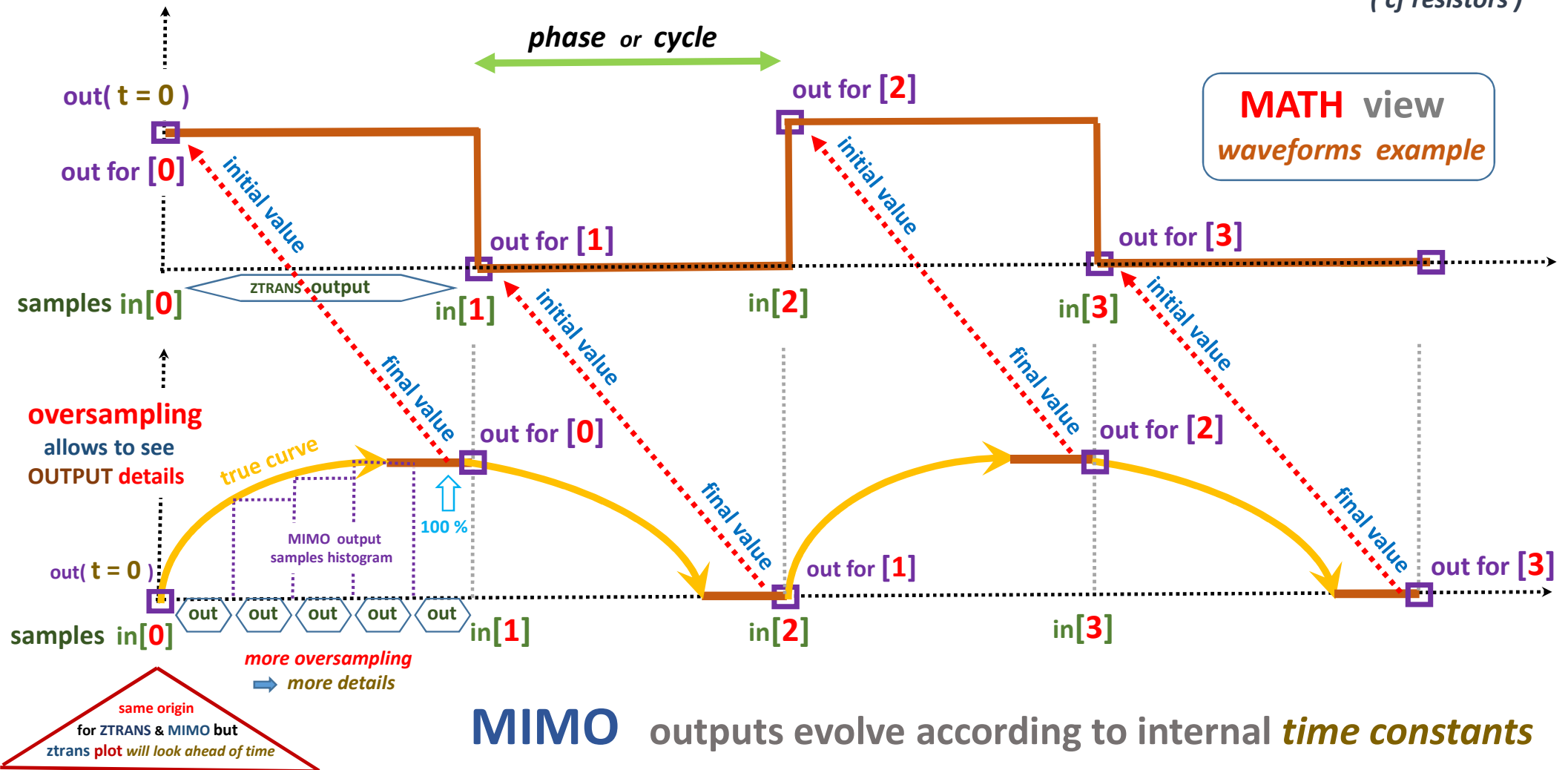
... time response ( cycle )

$$Out_0 = \frac{nIN_1 IN_0 + nIN_0 IN_{-1} - d_0 Out_{-1}}{d_1}$$

intracycle  
even index  
→ CLKb

== NOTE: CYCLE mode will not remain exact in case of intracycle INPUT changes due to CLKb coefficients =  $\boxed{IN_{-2}}$

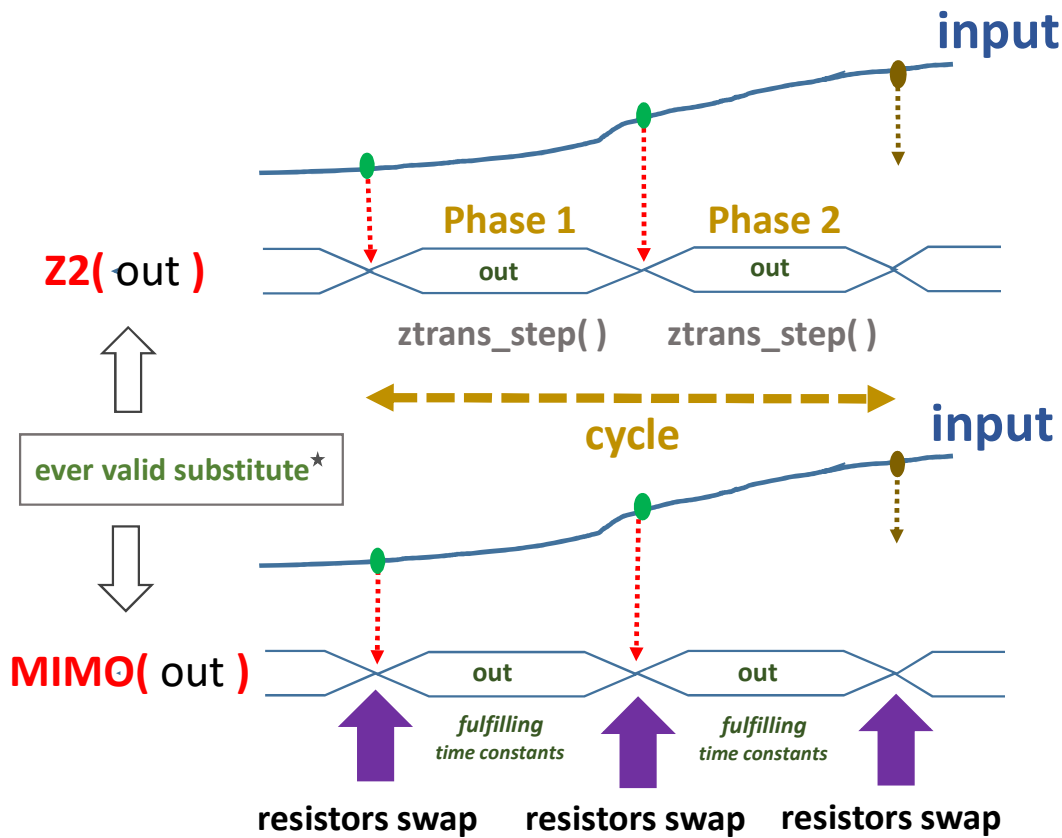
**ZTRANS** outputs evolve like **MIMO** would do if the **time constants** were removed  
( cf resistors )



# ZTRANS / MIMO COMPARISON

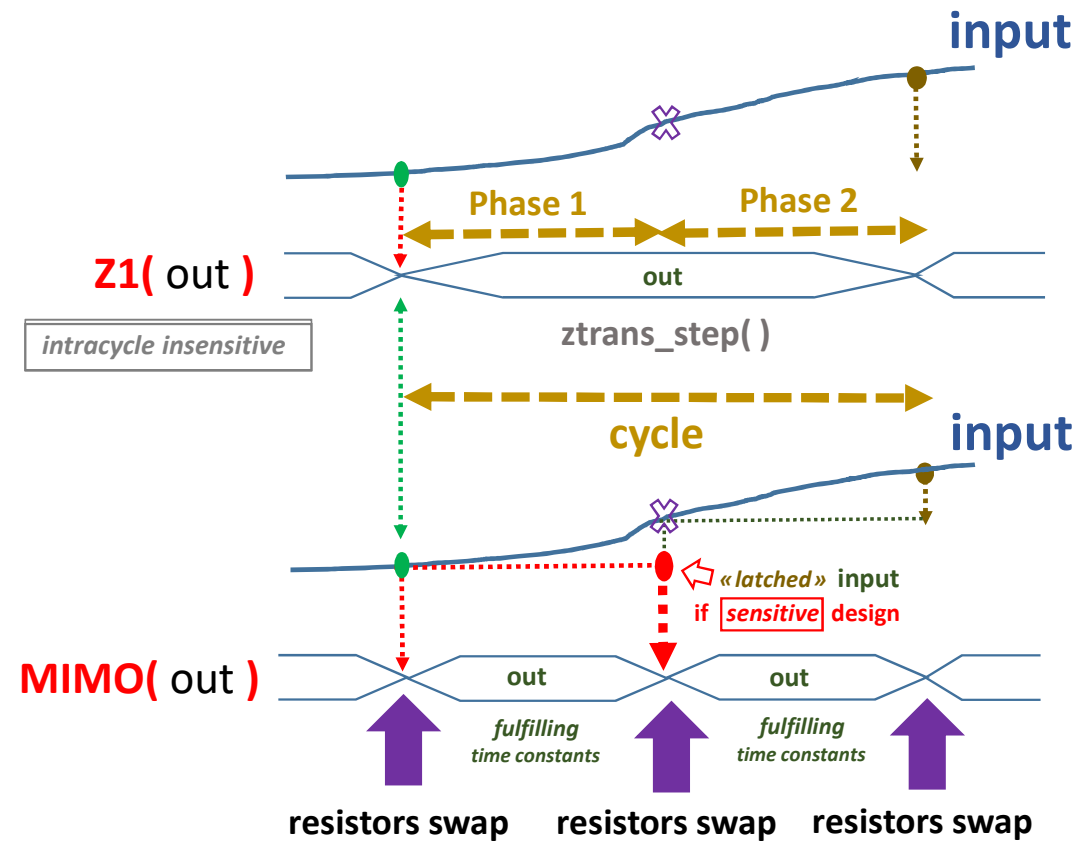
( basic case : cycle = 2 steps )

with MIMO PHASES



★ but possibly not identical due the MIMO analog time constants ( and/or slewrate )

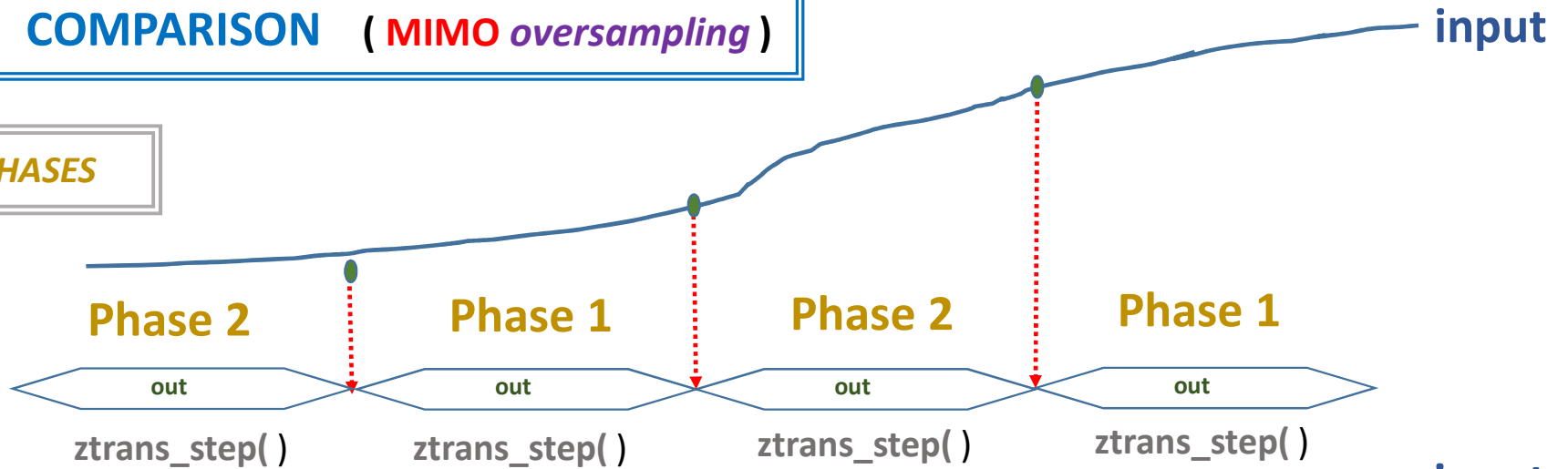
with MIMO CYCLE



# Z2 / MIMO COMPARISON (MIMO oversampling)

with MIMO PHASES

Z2( out )

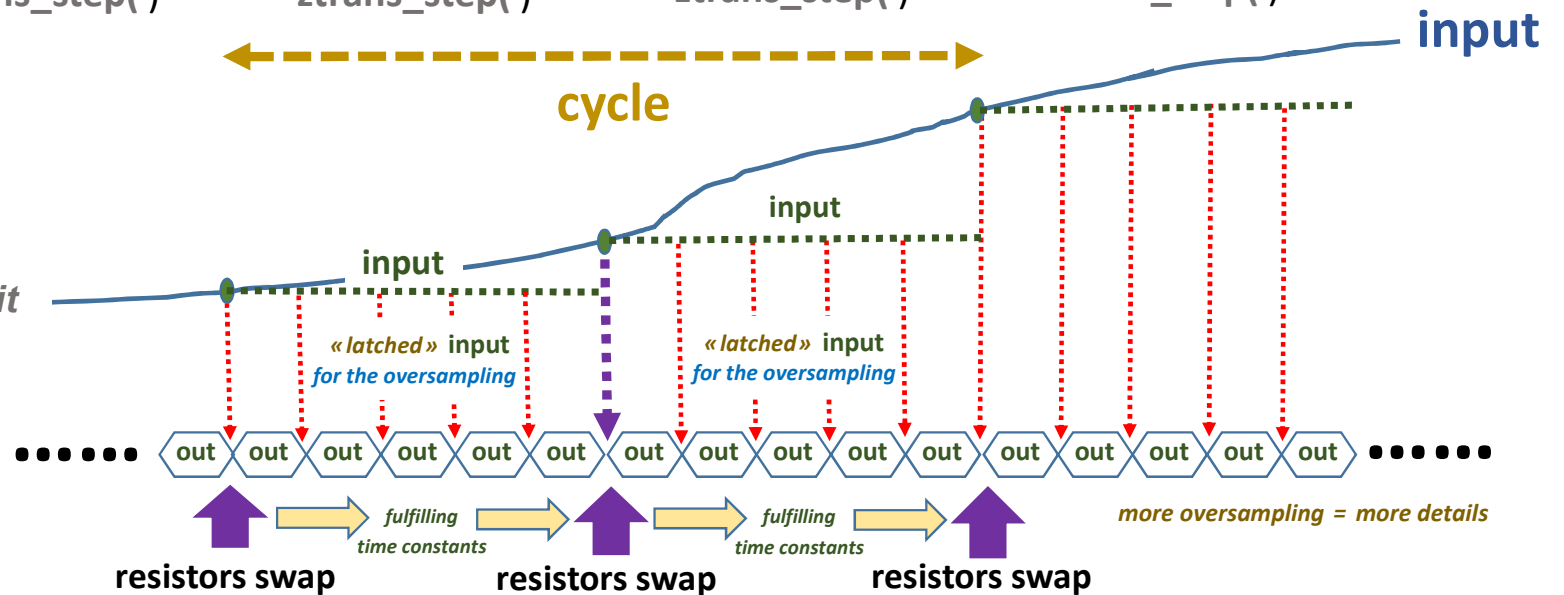


MIMO detailed curved line output  
modeled by Z squared output

« INTEGRATOR » type of circuit

MIMO( out )

OVERSAMPLING

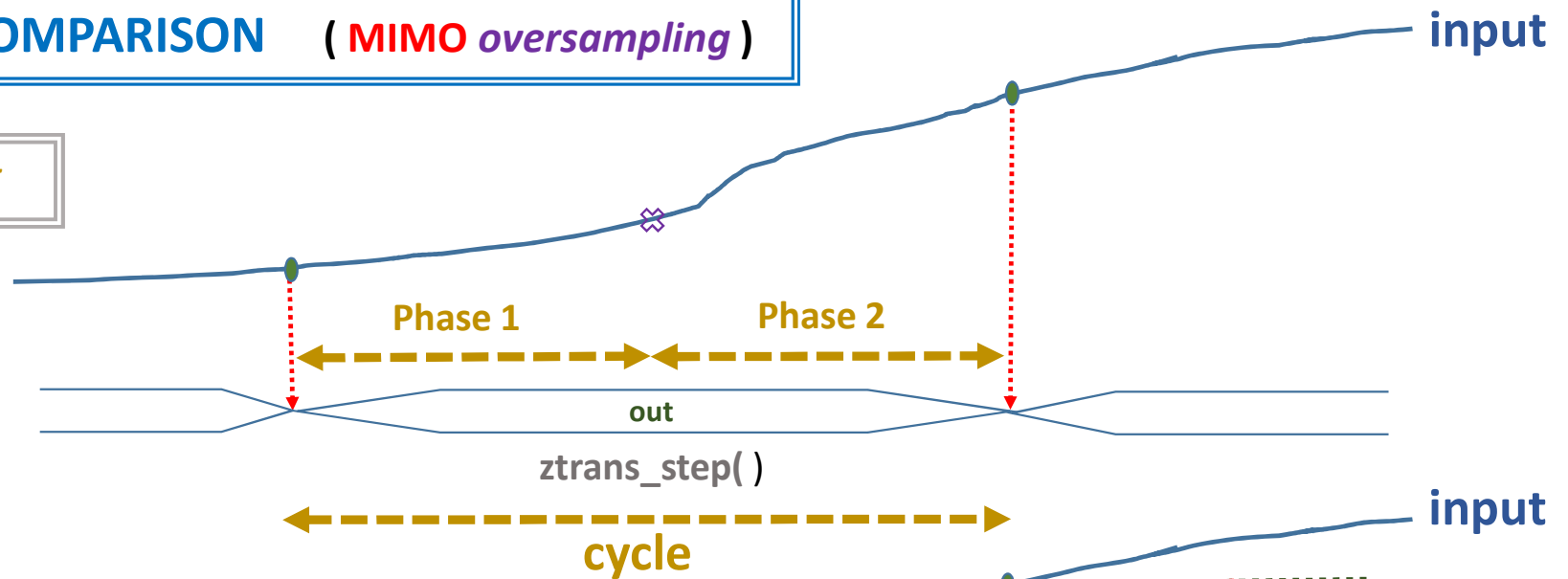


# Z1 / MIMO COMPARISON (MIMO oversampling)

with MIMO CYCLE

Z1( out )

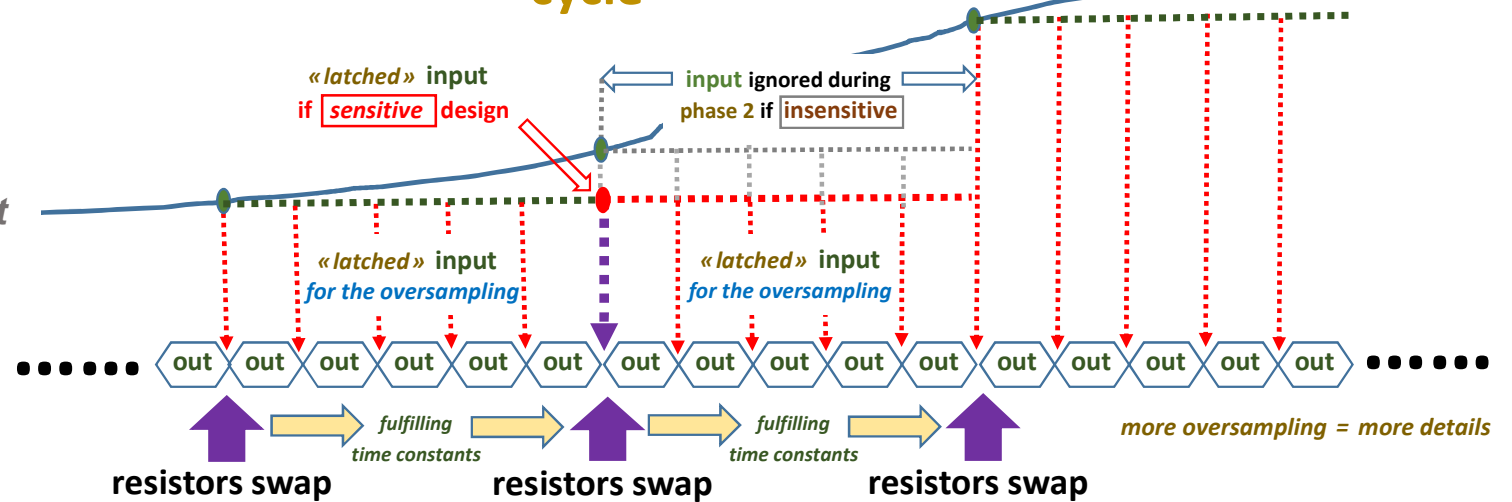
intracycle insensitive



MIMO detailed curved line output  
modeled by Z squared output

« INTEGRATOR » type of circuit

MIMO( out )  
OVERSAMPLING



# Comparison Z1( Out ) versus Z2( Out )

... time response ( cycle ) **one sampling and one output value per cycle** **Z1( Out )**

$$Out_0 = \frac{nOffs_1 \quad Offs_0 \quad +nVC2_1 \quad VC2_0 \quad +nOffs_0 \quad Offs_{-1} \quad +nVC2_0 \quad VC2_{-1} \quad +nVin_0 \quad Vin_{-1} \quad -d_0 \quad Out_{-1}}{d_1}$$

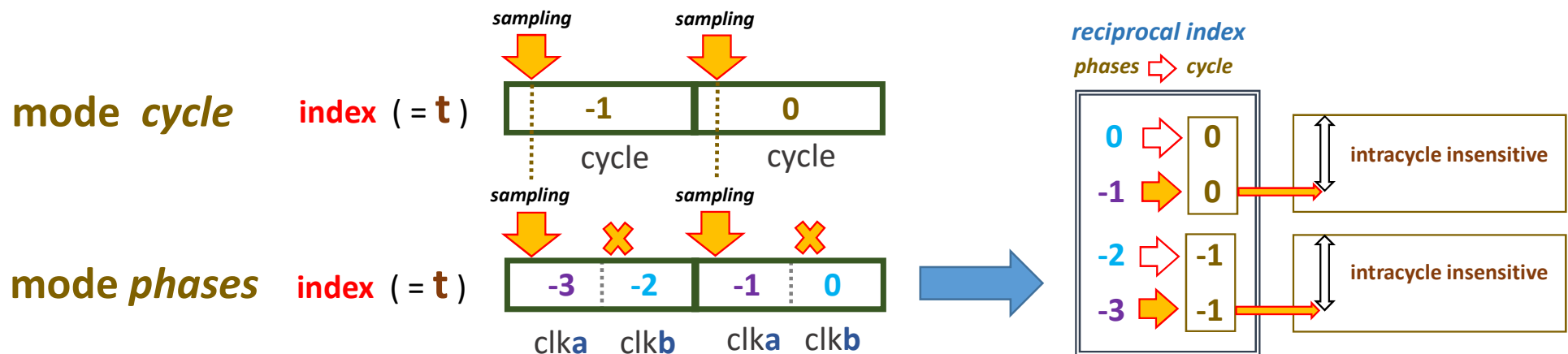
... time response ( when CLKa ) **irrelevant : cycle unique value masks any clka transient output** **Z2( Out )**

$$Out_0 = \frac{naOffs_2 \quad Offs_0 \quad +naVC2_2 \quad VC2_0 \quad +naVin_1 \quad Vin_{-1} \quad +naOffs_0 \quad Offs_{-2} \quad +naVC2_0 \quad VC2_{-2} \quad -da_0 \quad Out_{-2}}{da_2}$$

... time response ( when CLKb ) **equation of clk b output calculates by construct the final [ clka clk b ] output value**

$$Out_0 = \frac{nbOffs_2 \quad Offs_0 \quad +nbVC2_2 \quad VC2_0 \quad +nbOffs_1 \quad Offs_{-1} \quad +nbVC2_1 \quad VC2_{-1} \quad +nbOffs_0 \quad Offs_{-2} \quad +nbVC2_0 \quad VC2_{-2} \quad +nbVin_0 \quad Vin_{-2} \quad -db_0 \quad Out_{-2}}{db_2}$$

this expression plotted all along the cycle = Z1( Out )





# Comparison Z1( Out ) versus Z2( Out )

... time response ( cycle )

one sampling and one output value per cycle

Z1( Out )

$$Out_0 = \frac{nOffs_1 \quad Offs_0 \quad +nVC2_1 \quad VC2_0 \quad +nOffs_0 \quad Offs_{-1} \quad +nVC2_0 \quad VC2_{-1} \quad +nVin_0 \quad Vin_{-1} \quad -d_0 \quad Out_{-1}}{d_1}$$

... time response ( when CLKa )

irrelevant : cycle unique value masks any clka transient output

Z2( Out )

$$Out_0 = \frac{naOffs_2 \quad Offs_0 \quad +naVC2_2 \quad VC2_0 \quad +naVin_1 \quad Vin_{-1} \quad +naOffs_0 \quad Offs_{-2} \quad +naVC2_0 \quad VC2_{-2} \quad -da_0 \quad Out_{-2}}{da_2}$$

... time response ( when CLKb )

equation of clk output calculates by construct the final [ clka clk b ] output value

$$Out_0 = \frac{nbOffs_2 \quad Offs_0 \quad +nbVC2_2 \quad VC2_0 \quad +nbOffs_1 \quad Offs_{-1} \quad +nbVC2_1 \quad VC2_{-1} \quad +nbOffs_0 \quad Offs_{-2} \quad +nbVC2_0 \quad VC2_{-2} \quad +nbVin_0 \quad Vin_{-2} \quad -db_0 \quad Out_{-2}}{db_2}$$

this expression plotted all along the cycle = Z1( Out )

intracycle insensitive

internal cycle

cycle / cycle shift

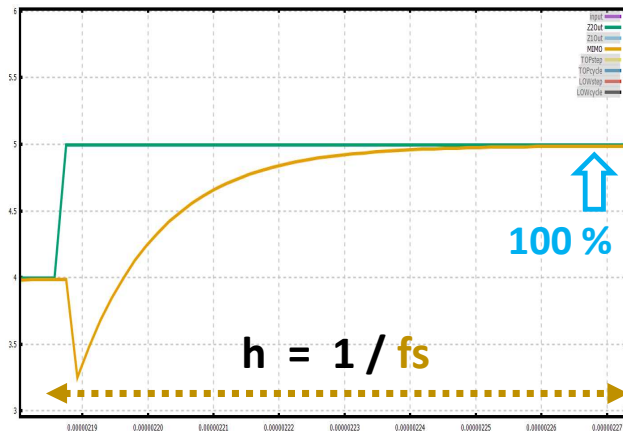
Offs <sub>-1</sub> → Offs <sub>0</sub>	VC2 <sub>-1</sub> → VC2 <sub>0</sub>	Vin <sub>-1</sub> <small>not present in above expression</small>	
Offs <sub>-2</sub> → Offs <sub>-1</sub>	VC2 <sub>-2</sub> → VC2 <sub>-1</sub>	Vin <sub>-2</sub> → Vin <sub>-1</sub>	Out <sub>-2</sub> → Out <sub>-1</sub>

by construction there is no possible Out<sub>-1</sub> coefficient  
clk b is not using clka output as one of its inputs

$$Out_0 = \frac{(nbOffs_2 + nbOffs_1) \quad Offs_0 \quad + (nbVC2_2 + nbVC2_1) \quad VC2_0 \quad + nbOffs_0 \quad Offs_{-1} \quad + nbVC2_0 \quad VC2_{-1} \quad + nbVin_0 \quad Vin_{-1} \quad -db_0 \quad Out_{-1}}{db_2}$$

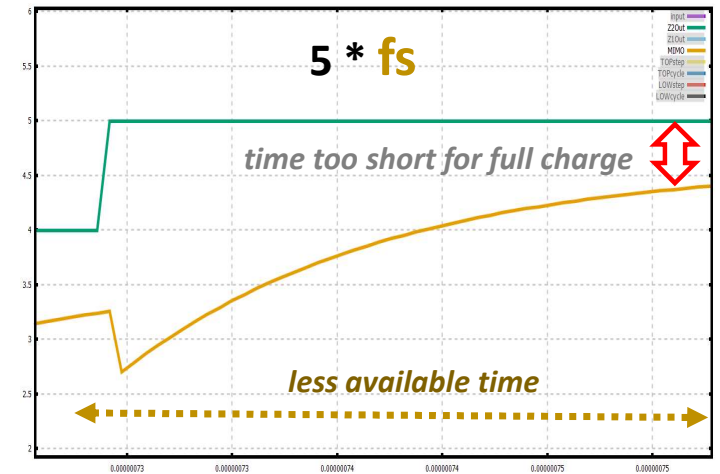


$fs \approx \text{function}(\text{rate of decay})$

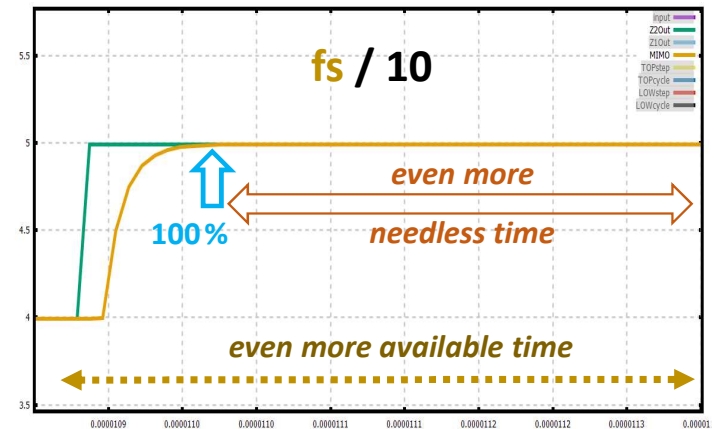
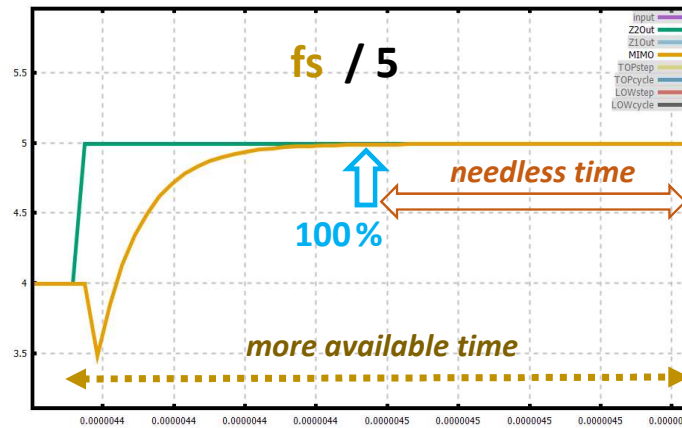


when  $fs$    
 charge < 100 %

charge MIMO < ZTRANS = 100 %



when  $fs$    
 visual aspect   
 MIMO   
 ZTRANS



Globals

```
%phases = [ PH1a , PH1b ]
%zshort = RDS
%printpoles = 2
k
AV
Vmax
```

rate of decay **a**

```
>>> SARC Z_Integrator -> i1 -> POLES
POLES : matrix(
[ -1.67226124659431225154548883438110E+04 , +0.0000000000000000000000000000E+00 ] ,
[ -8.01445909870613068342208862304688E+07 , +0.0000000000000000000000000000E+00 ] ,
[ -2.0000000000000000000000000000000000E+20 , +0.0000000000000000000000000000E+00 ] ,
[ -5.0049998000409913851904000000000000E+23 , +0.0000000000000000000000000000E+00 ] ) ;
```

*REAL part*

*frequency part*

```
>>> SARC Z_Integrator -> i1 -> POLES
POLES : matrix(
[ -1.67226124659431225154548883438110E+04 , +0.0000000000000000000000000000E+00 ] ,
[ -8.01445909870613068342208862304688E+07 , +0.0000000000000000000000000000E+00 ] ,
[ -2.0000000000000000000000000000000000E+20 , +0.0000000000000000000000000000E+00 ] ,
[ -5.0049998000409913851904000000000000E+23 , +0.0000000000000000000000000000E+00 ] ) ;
```

$$e^{-a t} = e^{-t / \tau}$$

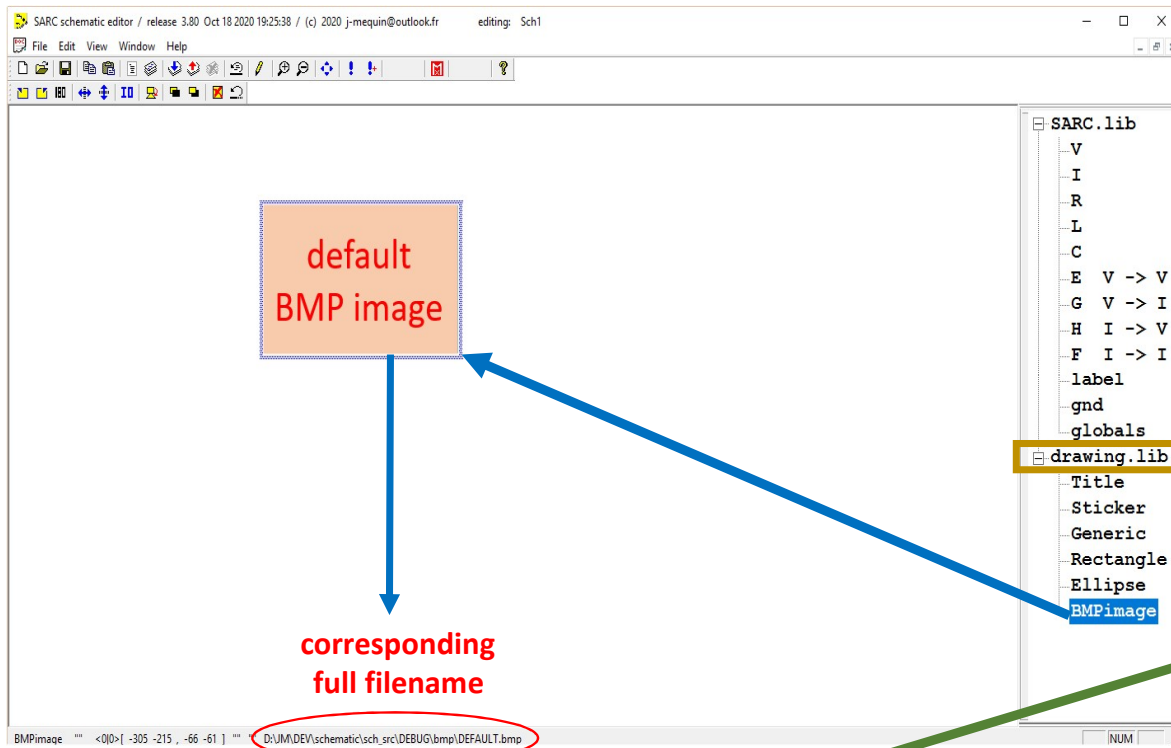
$$\tau = \frac{1}{a} \approx 35 \% \text{ full charge time}$$

$$10 \tau \Rightarrow e^{-1/10} \approx 90 \%$$

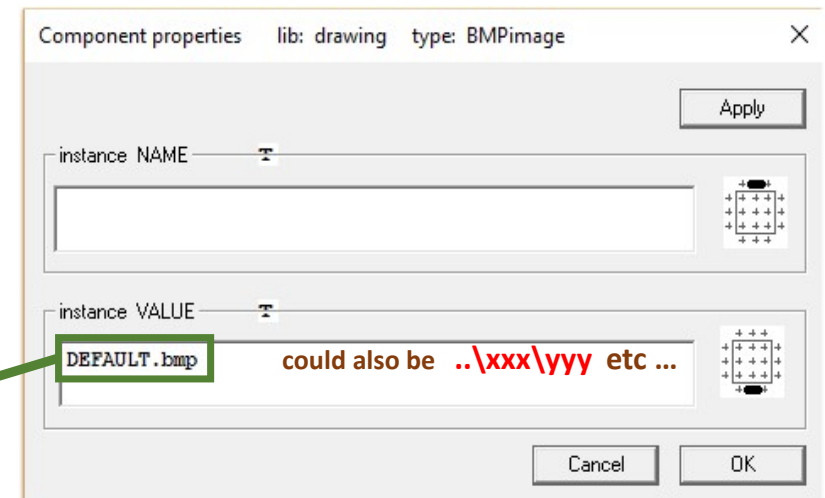
$$f_s \approx \frac{a}{10} \text{ for } 90 \%$$

$$n = -1 / \ln( \% )$$

5 is a recommended rule of thumb



## BMP image insertion

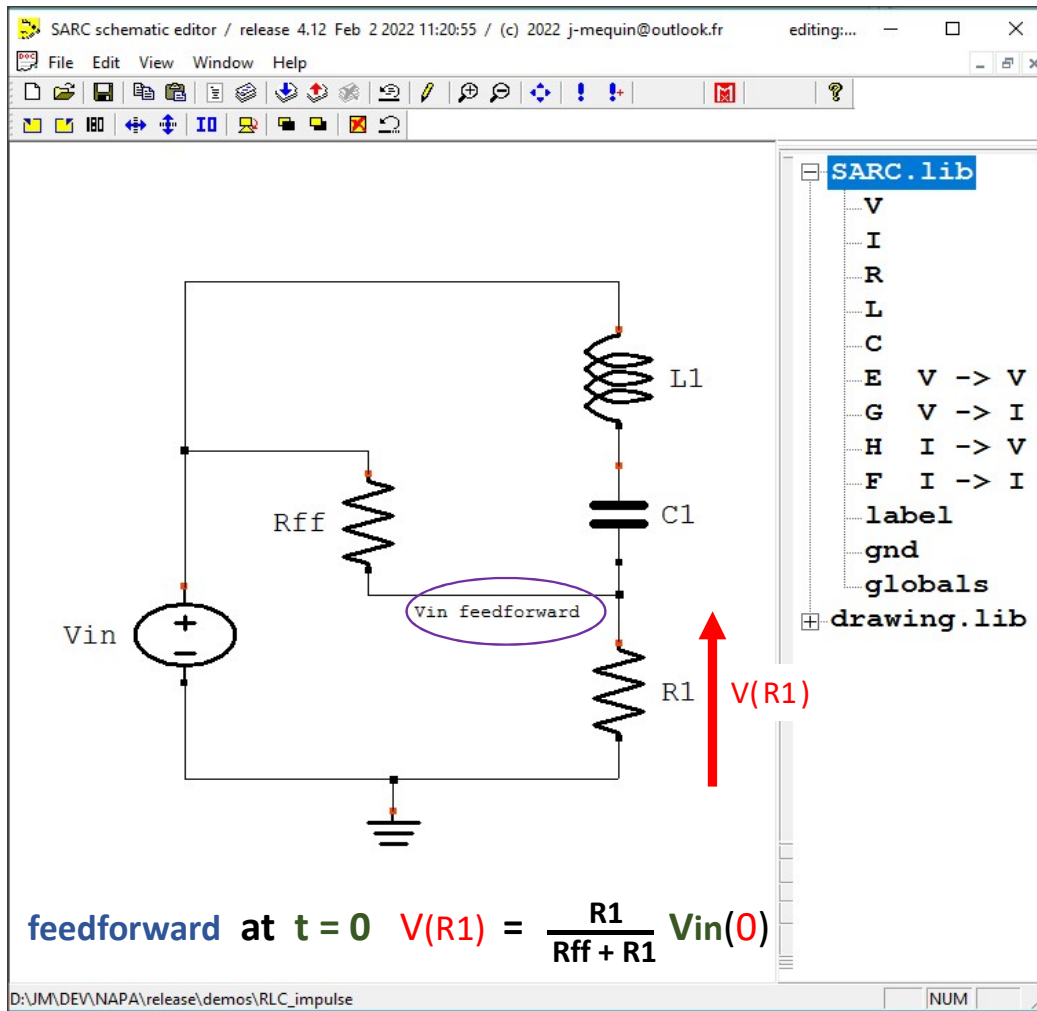


*can be replaced with*

- a **filename** that can be found in the **document folder** ( document must have been already saved at least once )
- a **filename** that can be found in the **schematic editor installation bmp/ folder** ( = visible by all documents )
- a **full filename**

# *impulse response*

standalone «C» validation model



SARC setup

INTERN

OUTPUTS `V( R1 )`

execution order  GENERATE\_XFER( ☐ nointern )

execution order  GENERATE\_MIMO

showxfer ☒ XWISH

`napamode : false ;`

`GENERATE_MIMO( ) ;`

User code

Maxima

**ANALOG\_VIEW : false** ➡ **MATH**

```

RLC_impulse.c

#include <stdio.h>
#include "SARC_api.h"
#include "RLC_impulse_mimo.h"

/*-----*/
double L1      = 100E-3 ;
double C1      = 100E-9 ;
double R1      = 100    ;
double Rff     = 1E5    ;
/*-----*/
double dirac   = 1E6    ;
int samples    = 5000   ;
/*-----*/

int main( )
{
    FILE *fgnuplot = fopen( "fplot" , "w" ) ;

    double t      = 0      ;
    double h      = 1 / dirac ;
    double Vin    = 0      ; double normalize = R1 / L1 ; /* max output */

    pSARC psarc = SARC_ALLOC( MIMO_RLC_impulse( ) , "i1" ) ;

    double U[ 1 ] ; double *lookup_INPUTS[ ] = { &U[0] } ;
    double Y[ 1 ] ; double *lookup_OUTPUTS[ ] = { &Y[0] } ;
    double *lookup_BOM[ ] = { &L1 , &C1 , &R1 , &Rff } ;

    psarc->lookup_h      = &h ;
    psarc->lookup_INPUTS = &lookup_INPUTS[ 0 ] ;
    psarc->lookup_OUTPUTS = &lookup_OUTPUTS[ 0 ] ;
    psarc->lookup_BOM     = &lookup_BOM[ 0 ] ;

    for ( int n = 0 ; n < samples ; n++ )
    {
        if ( t == 0 ) Vin = dirac ;
        else Vin = 0 ;

        SARC_STEP_Tminus( psarc ) ;
        U[ 0 ] = Vin ; SARC_STEP_Tplus( psarc ) ;

        fprintf( fgnuplot , "%E %E %E\n" , t , U[0] , Y[0] / normalize ) ;

        t = t + h ;
    }

    return 0 ;
}

```

**dirac (single step)** ←

$$\mathbf{A} = \begin{bmatrix} -\frac{R1 Rff}{L1 (Rff + R1)} & -\frac{1}{L1} \\ \frac{1}{C1} & 0 \end{bmatrix}$$

$$\mathbf{B} = \begin{bmatrix} \frac{Rff}{L1 (Rff + R1)} \\ 0 \end{bmatrix}$$

$$\mathbf{C} = \begin{bmatrix} \frac{R1 Rff}{Rff + R1} & 0 \end{bmatrix}$$

$$\mathbf{D} = \frac{R1}{Rff + R1}$$

feedforward

```

gnuplot
File Plot Expressions Functions General Axes Chart Styles 3D Help
Replot Open Save ChDir Print PRTSc Prev Next Options

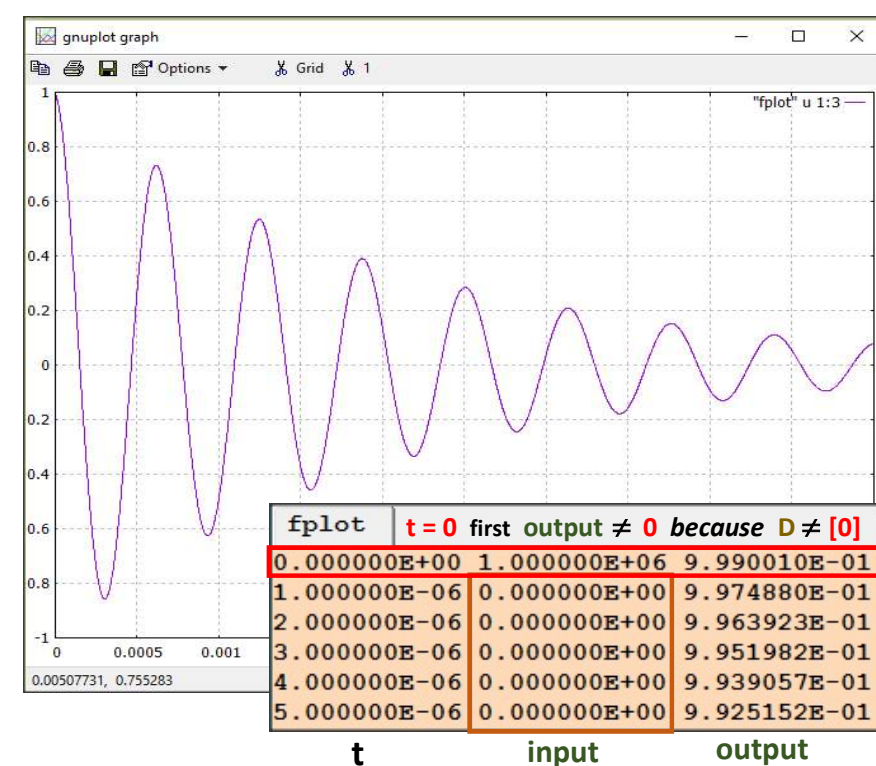
GNU PLOT
Version 5.0 patchlevel 6 last modified 2017-03-18

Copyright (C) 1986-1993, 1998, 2004, 2007-2017
Thomas Williams, Colin Kelley and many others

gnuplot home: http://www.gnuplot.info
faq, bugs, etc: type "help FAQ"
immediate help: type "help" (plot window: hit 'h')

Terminal type set to 'windows'
gnuplot> cd "/jm/dev/napa/release/demos/RLC_impulse"
gnuplot> plot "fplot" u 1:3 w l
gnuplot>

```





# *APPENDIX*

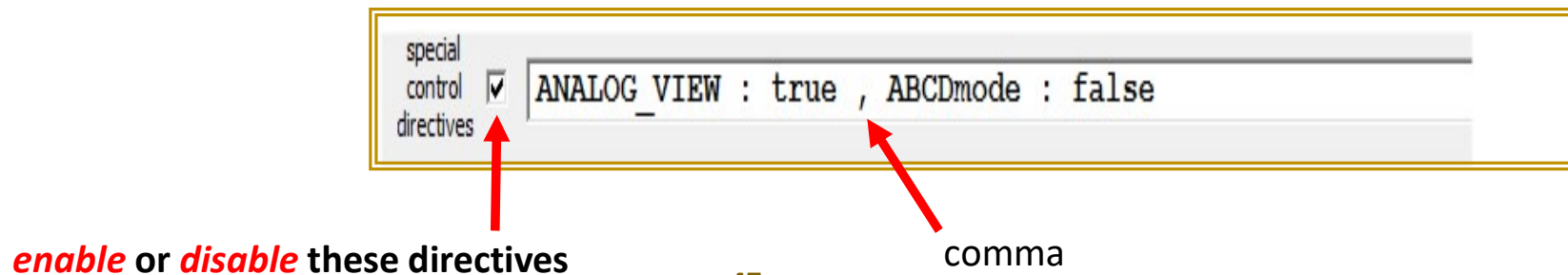
The **wxPAUSE( )** function can be used to force a **pause** during the execution of a **wxMaxima** script

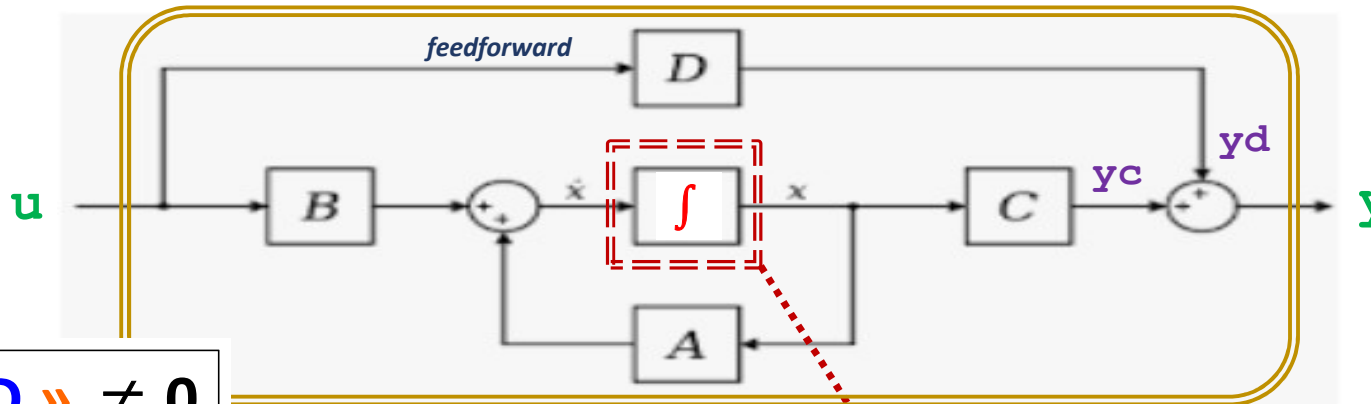
default SARC environment variables	default		
	napamode	: false ;	true / false
	ANALOG_VIEW	: false ;	true / false
	convention	: "PSC" ;	"PSC" / "GLC"
	ABCDmode	: true ;	true / false

or GCC compile option  
-DGCC\_ANALOG\_VIEW=0/1

*could be* redefined in the **Maxima** *initialisation environment file*

Or in a **SARC setup** pop up menu



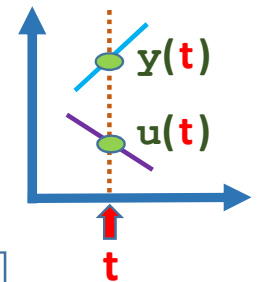


when «  $D$  »  $\neq 0$

mathematical  
response

$$y(t) = y_c(t) + y_d(t) = f_c(u(t-1)) + f_d(u(t))$$

zero delay dependency



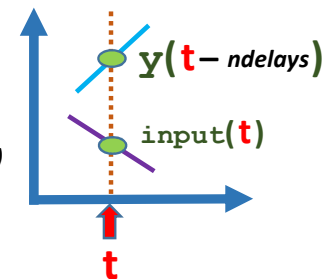
This is not an issue for the SARC validation environment that simulates standalone «  $C$  » model individually

but, independently of SARC, zero delay blocks are almost always **delayed**\* by simulators (including NAPA)

simulator  
response

$$y(t) = f_c(u(t-2)) + f_d(u(t-1))$$

this is ok  
but implies plots  
(imperceptible with small steps)

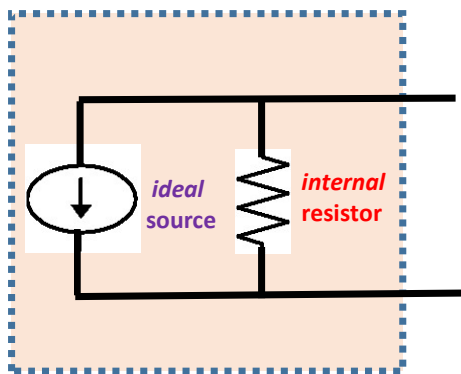
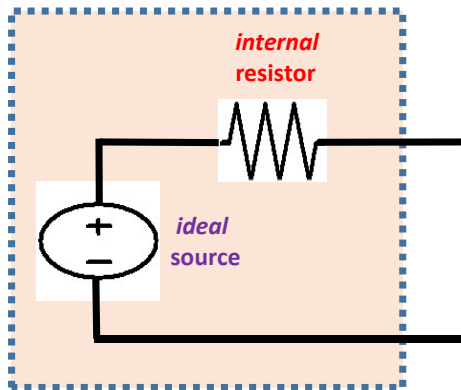


\* to prevent the eventuality of a zero delay assembly building a snake biting its own tail

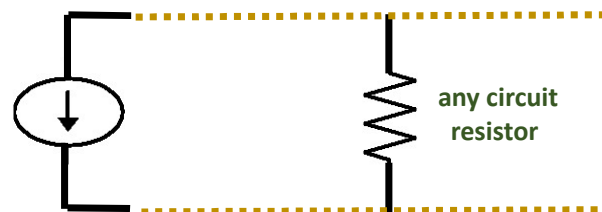
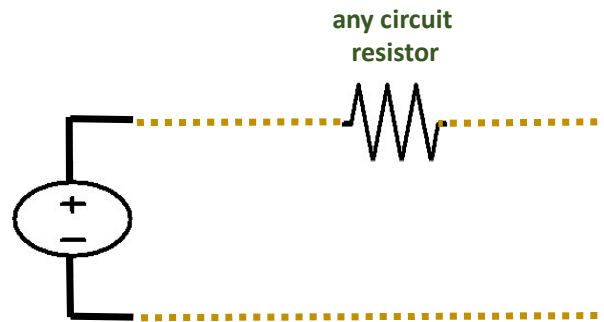
(regarding SARC the fact that  $D$  could be  $\neq 0$  should not qualify the block as "zero delay" since the feedforward is handled internally only once per step)



*academic*  
*physical* source

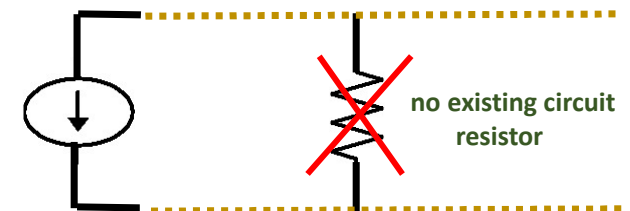
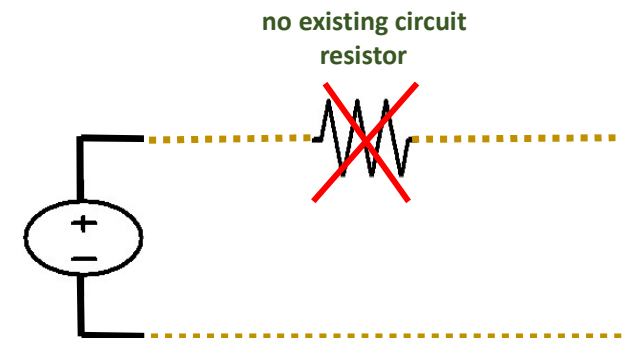


**SARC**  
*proper* source



**SARC**  
*boundless* source

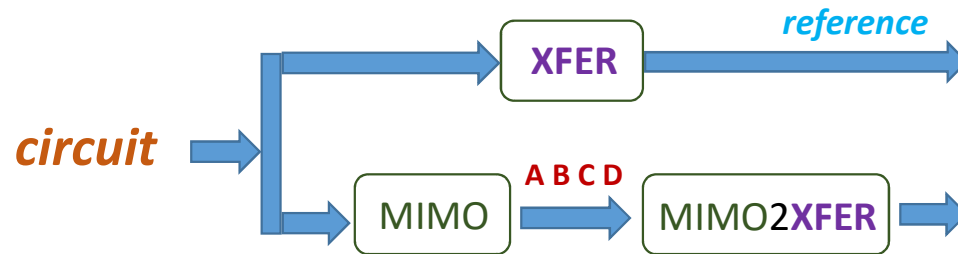
**NO RESISTOR → NO TIME CONSTANT**



# QC methods

for « *healthy* » outputs ( without *Warnings* )

1 )



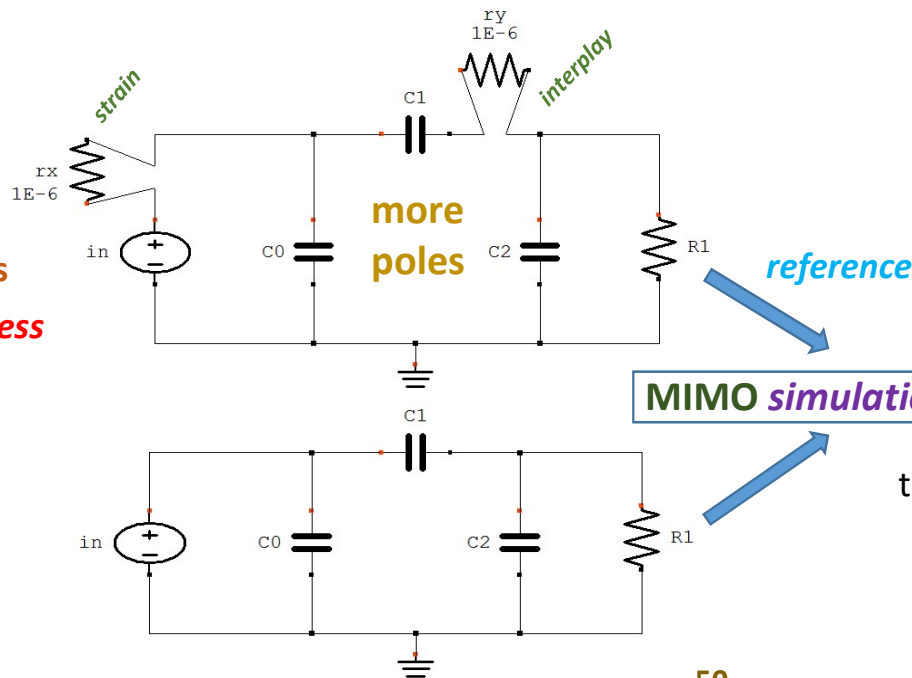
??? *transfer functions* should be *the same*

this verifies that **A B C D** are the **correct ones**

2 )

updated circuit  
with **small** resistors  
to eliminate **ALL boundless**

( *strain and interplay* )



??? *plots* should be *the same*

this verifies that the “*boundless*” are **well handled**

## MIMO status variables

---

NULL = DEGEN + AKIN ( degenerated states are toxic for circuit state matrix invertibility )

DEGEN "degenerated" states

\* when several C are forming a mesh

one C voltage is therefore enslaved to the others ( KVL )

\* when several L have their respective current converging to an ISOLATED node

one L current is therefore enslaved to the others ( KCL )

In those configurations, it should be noted that a voltage source can also play the role of a C or a current source the role of a L

AKIN simplest kind of "degenerated" states : parallel C or serial L

same voltage for C ( ==>> redundant states )

or current for L ( ==>> redundant states )

COX collinear states resulting from ISOLATED serial C or parallel L

same current for C (  $I = C \, dV/dt = C \, dX/dt$  ==>> prorated states )

or voltage for L (  $V = L \, dI/dt = L \, dX/dt$  ==>> prorated states )

thus they cannot be counted as "degenerated" BUT they must be also discarded for state matrix invertibility

U2X boundless INPUT sources ( no R limiting maximum source throughput )

CS2X boundless controlled sources ( no R limiting maximum source throughput )

P2X PERCUSSION states reciprocal contribution

```

... NLC           : 3
... NESE          : 3
... NSTATES       : 1
... XWISH       : [C0,C2]

```

```

SERIAL []
PARALLEL [[C2,R1]]

```

```

STATES = [V(C2)]

```

```

ESE = [ [C0]
        [C1]
        [C2]
      ]

```

```

A = [ - 1 / ((C2 + C1) R1) ]
B = [ - C1 / ((C2 + C1) ^ 2 R1) ]

```

```

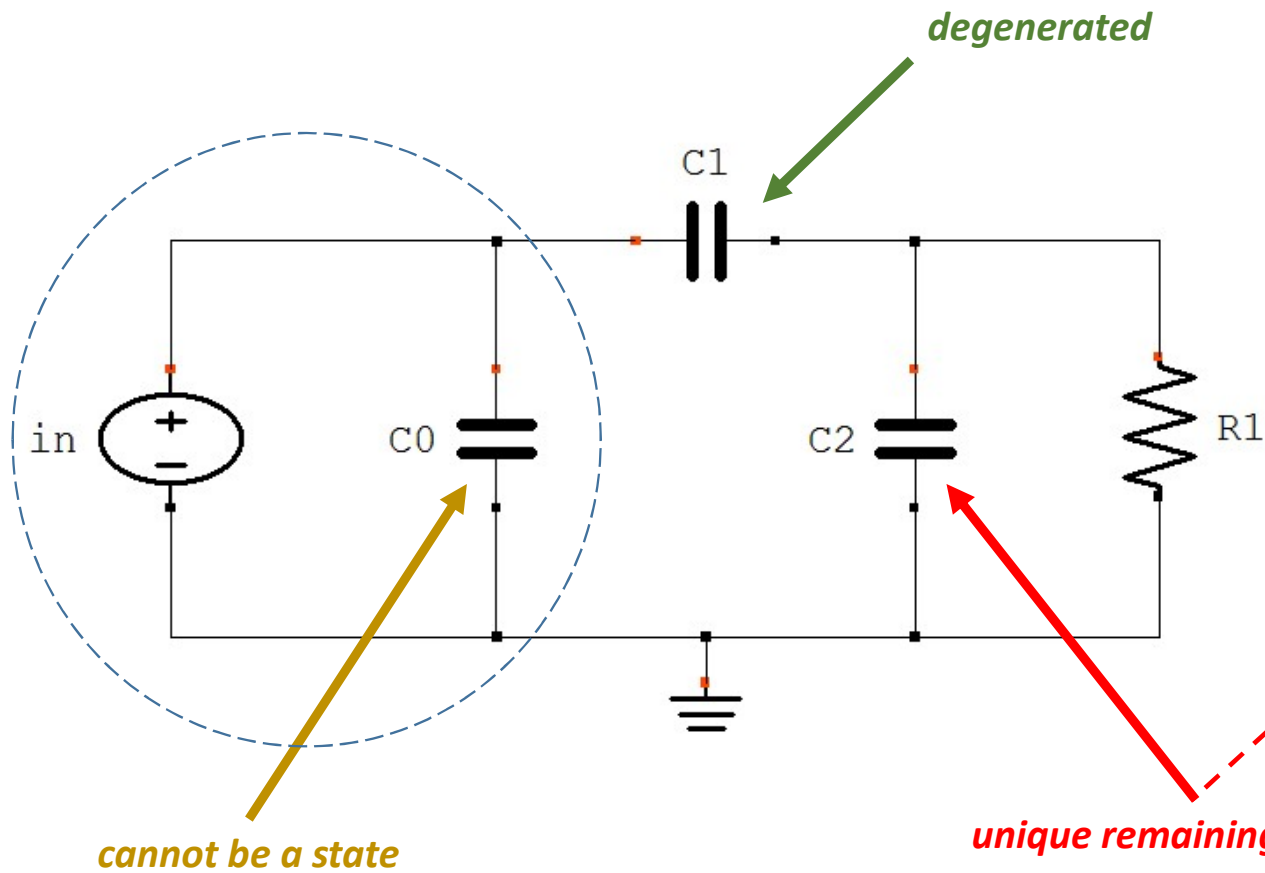
C = [ 0
      -1
      1
    ]

```

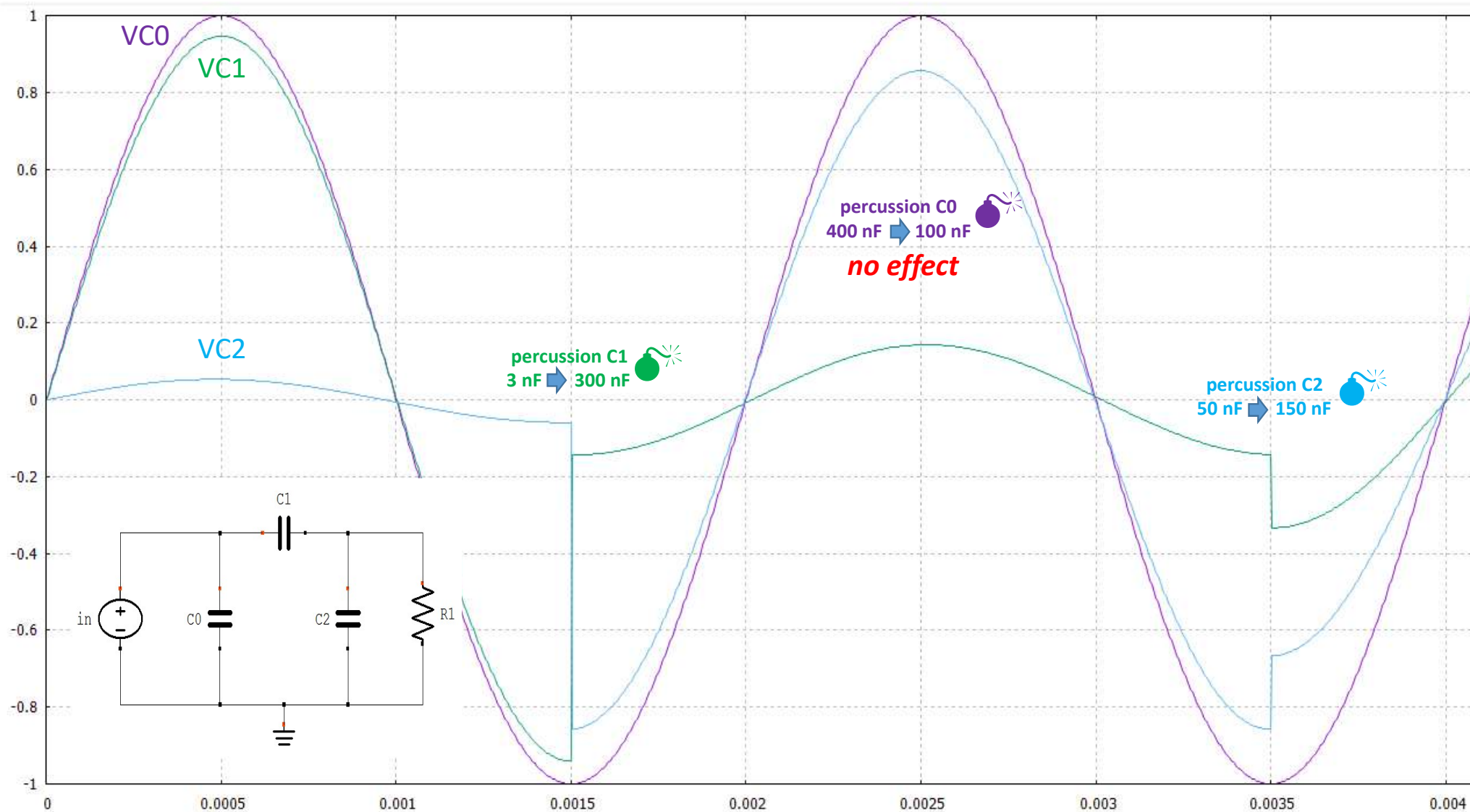
```

D = [ 1
      C2 / (C2 + C1)
      C1 / (C2 + C1)
    ]

```



OUTPUTS V( C0 ) , V( C1 ) , V( C2 )

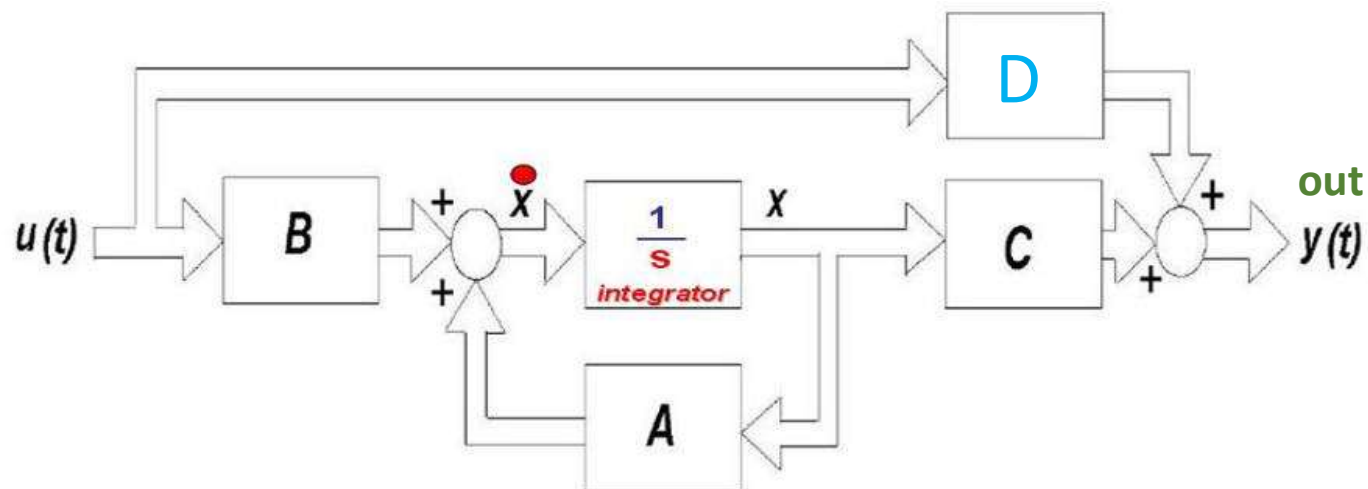
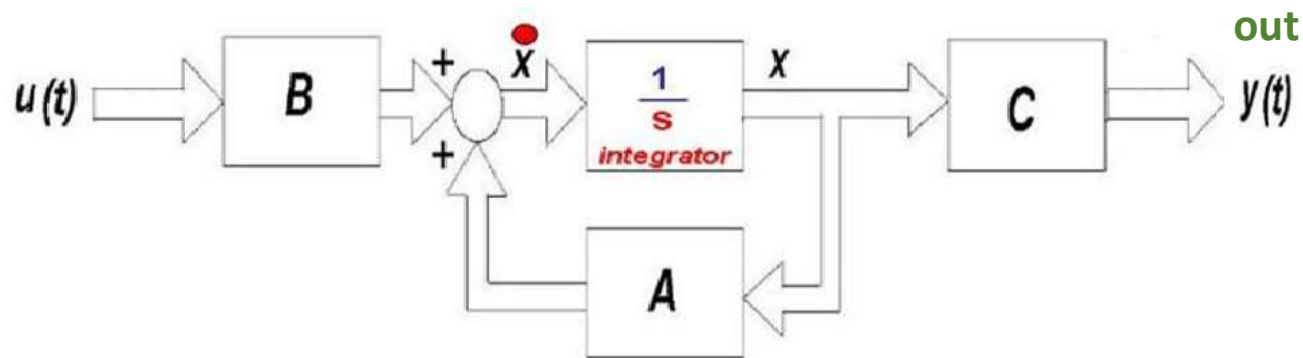


0.000144278, 0.634168

## MIMO2XFER

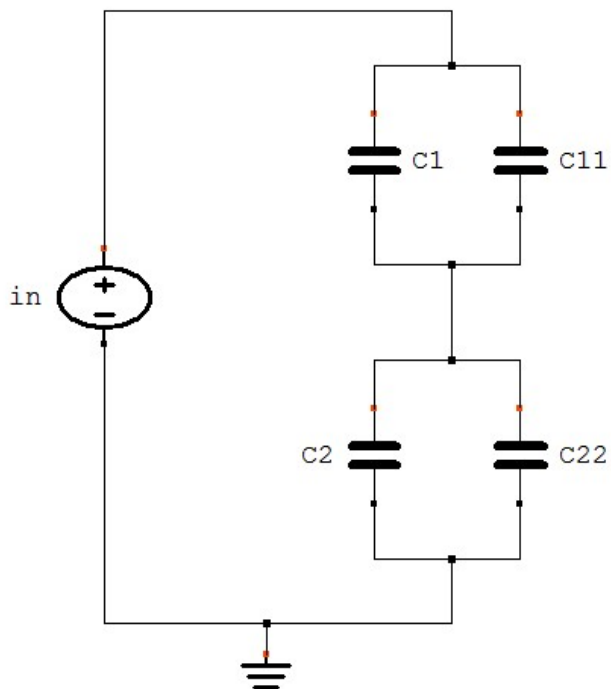
**PROPER** transfer function

$$D[\text{out}] = 0$$



**BIPROPER** transfer function

$$D[\text{out}] \neq 0$$



OUTPUTS V( C1 ) , V( C2 )

### GENERATE\_XFER

```
SERIAL []
PARALLEL [[C1,C11],[C2,C22]]

1 V(C1)/in =  $\frac{C22+C2}{C22+C2+C11+C1}$ 
2 V(C2)/in =  $\frac{C11+C1}{C22+C2+C11+C1}$ 
```

no |s| term ↔ no pole

### GENERATE\_MIMO

```
SERIAL []
PARALLEL [[C1,C11],[C2,C22]]
STATES=none
```

$$ESE = \begin{bmatrix} [C1, C11] \\ [C2, C22] \end{bmatrix}$$

$$D = \begin{bmatrix} \frac{C22+C2}{C22+C2+C11+C1} \\ \frac{C11+C1}{C22+C2+C11+C1} \end{bmatrix}$$

no state ↔ no eigenvalue  
only D feedforward matrix

**MIMO2XFER**  $XFER = C ( |s| I - A )^{-1} B + D$

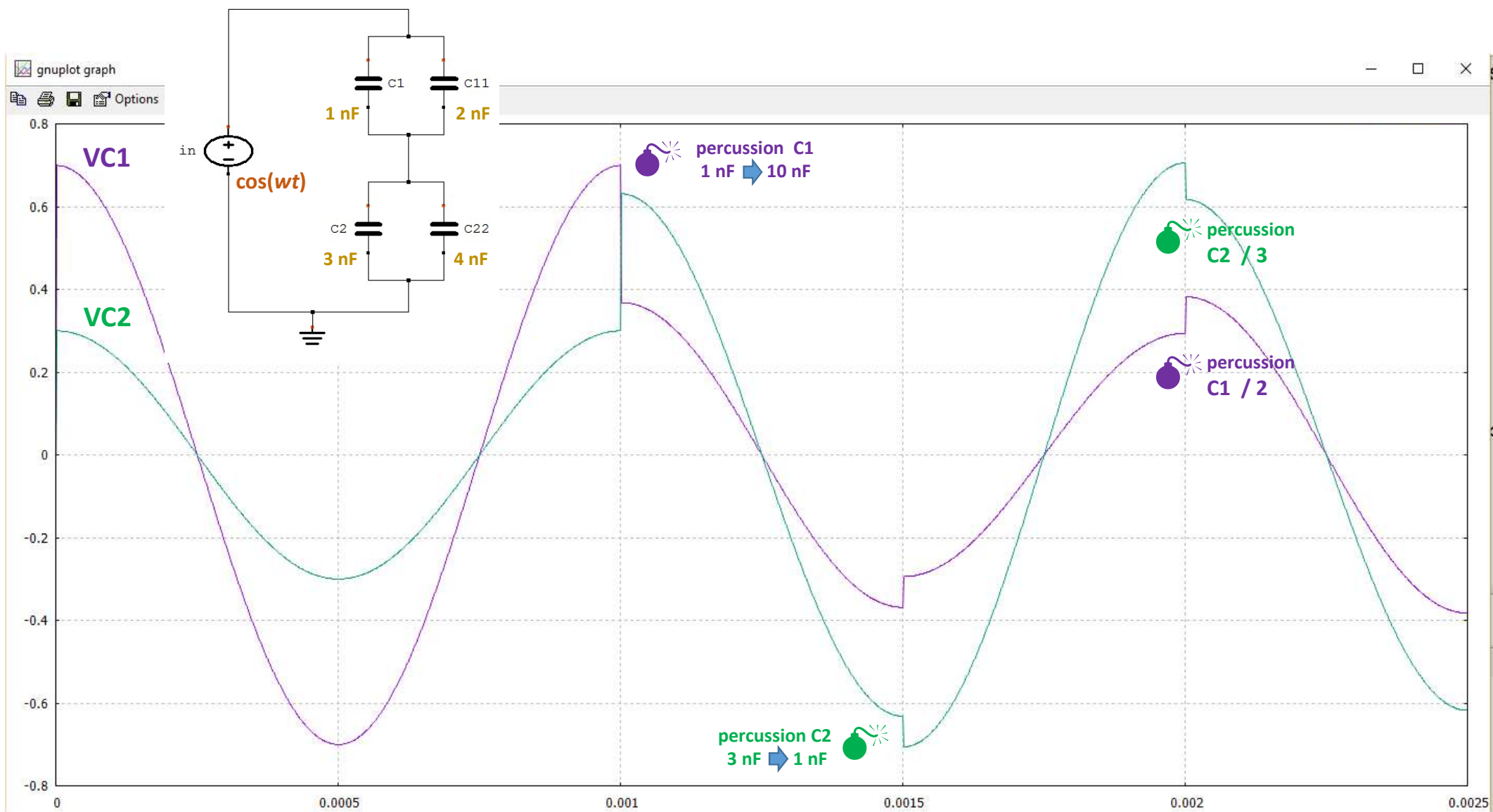
... INPUTS : [in] OMITTED : n/a

... OUTPUTS : [V(C1),V(C2)]

$$1 \quad V(C1)/in = \frac{C22+C2}{C22+C2+C11+C1}$$

$$2 \quad V(C2)/in = \frac{C11+C1}{C22+C2+C11+C1}$$





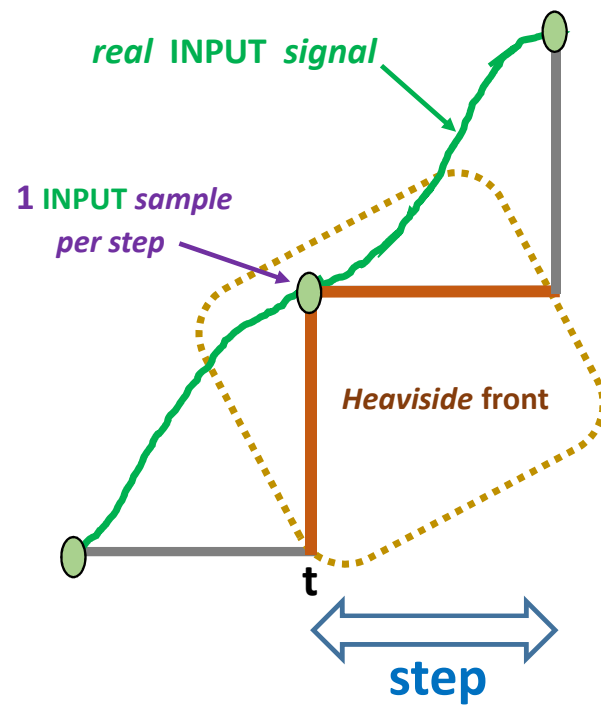


# *MATH/ANALOG* VIEW

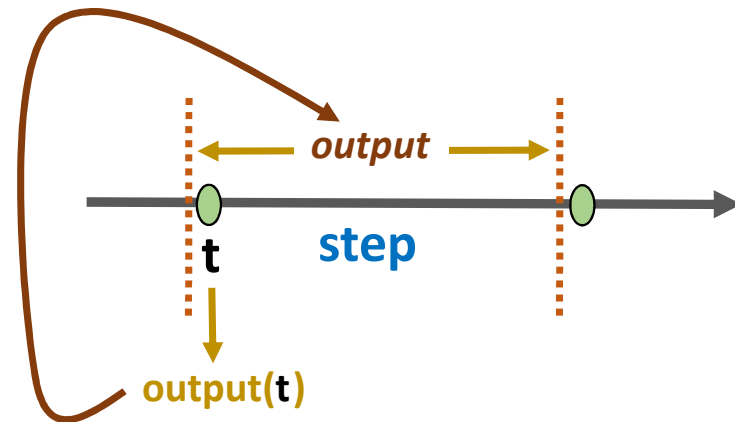
# CLASSICAL SIMULATION

( almost always not accepting "on fly" component value change )

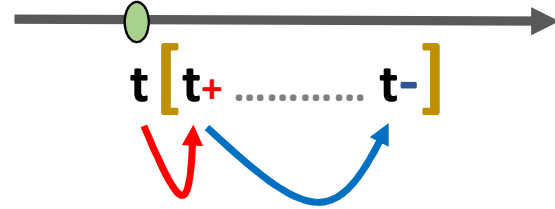
1 INPUT sample → 1 OUTPUT data



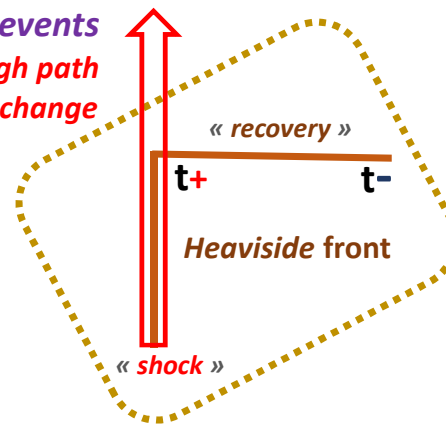
1 plot per step



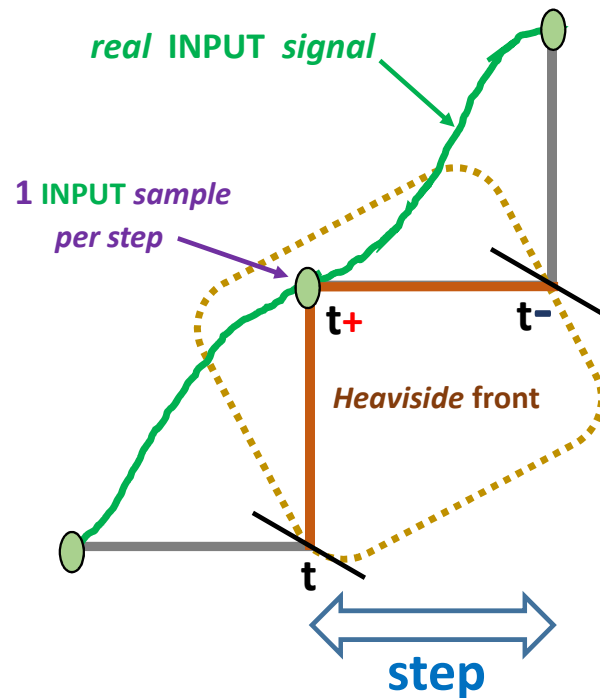
1 INPUT sample → 2 OUTPUT data



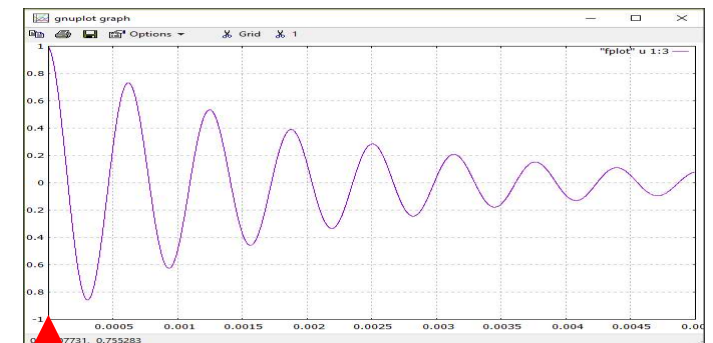
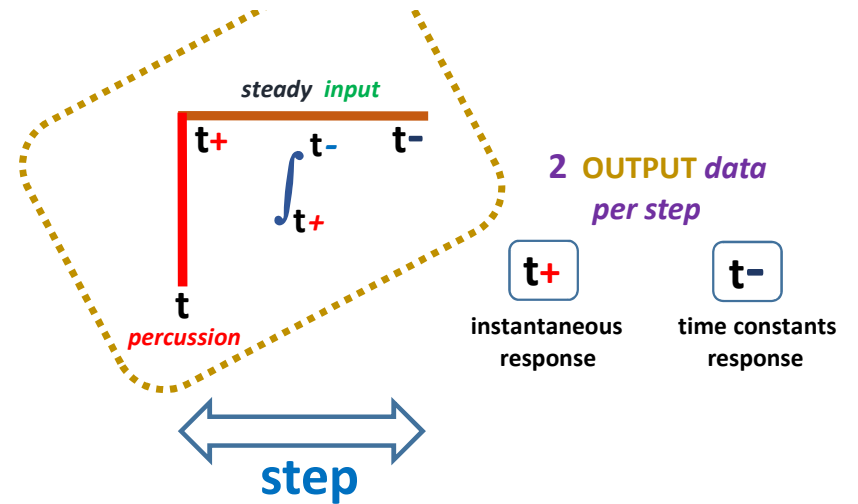
singular events  
direct feedthrough path  
or / and component(s) value change



2 consecutive algorithms



# SARC SIMULATION



shock ..... recovery

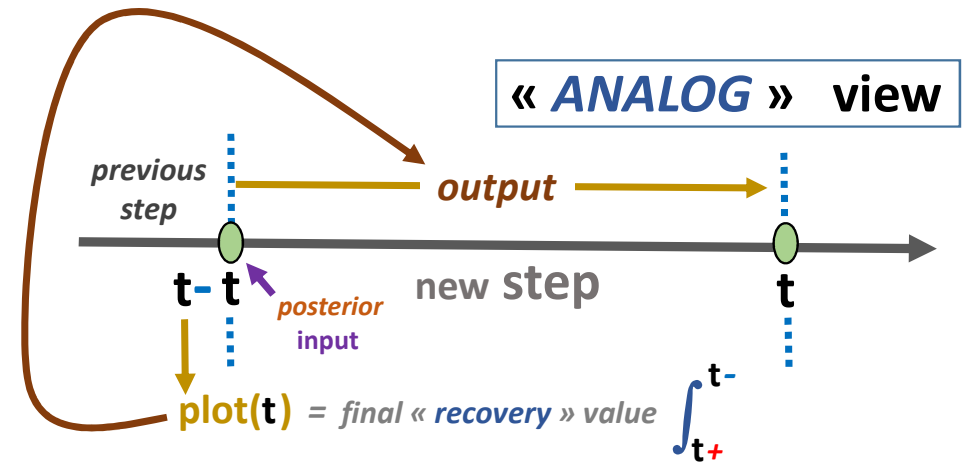
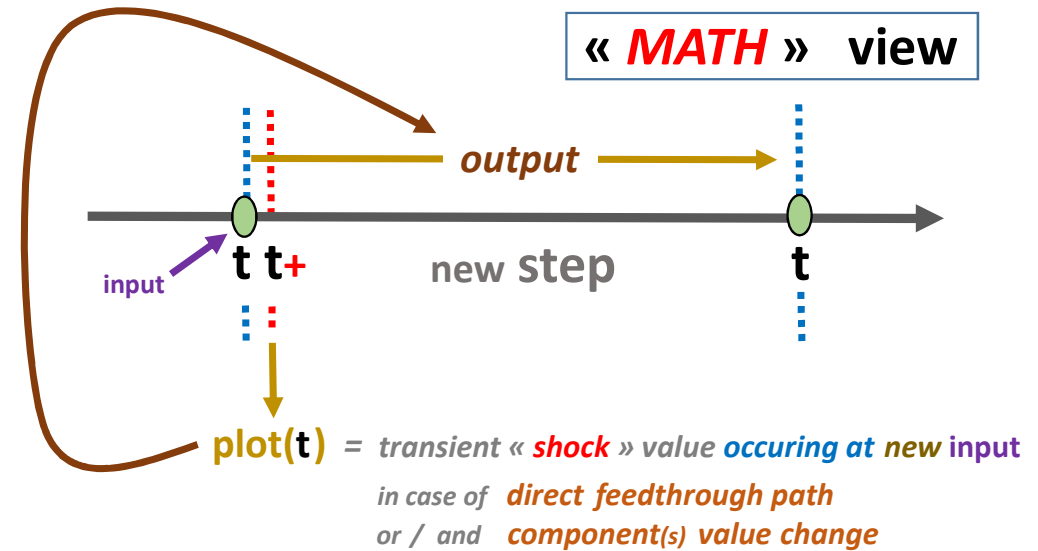
# SARC SIMULATION

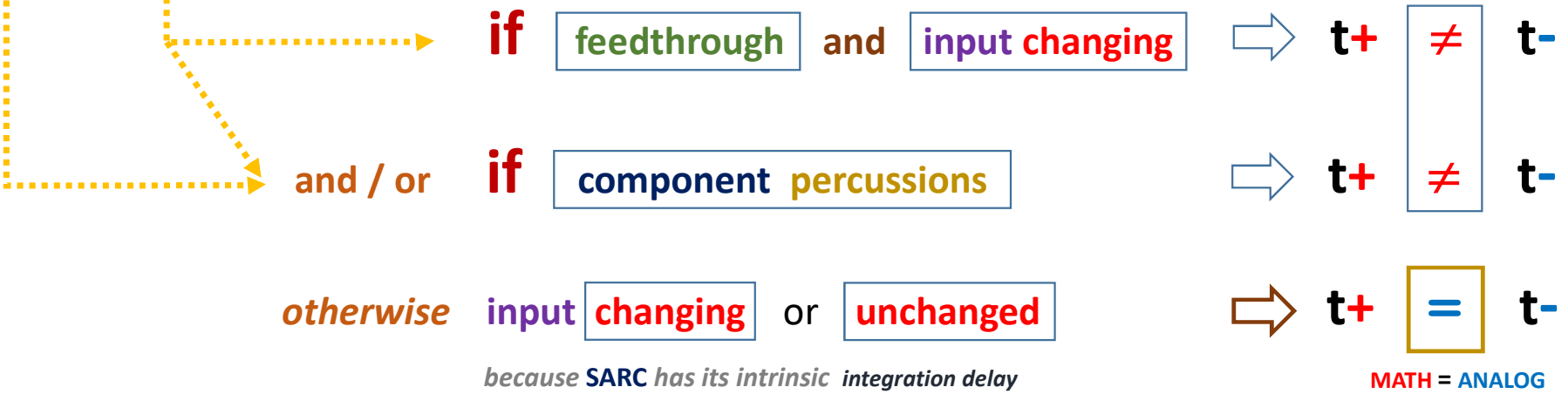
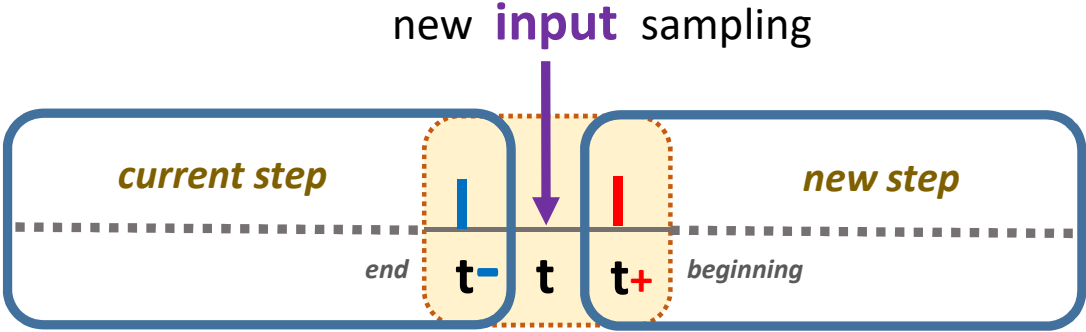
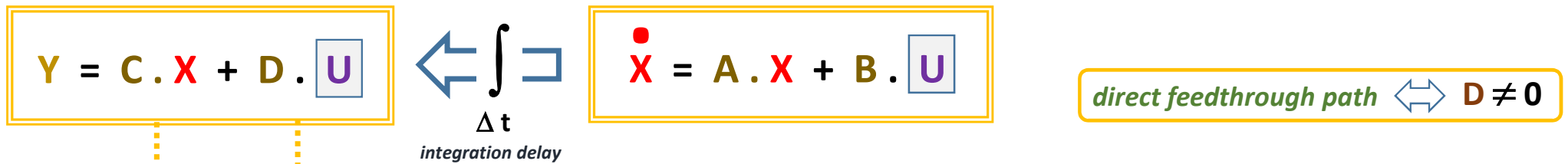
1 plot per step

The VIEW is a user choice that **does not affect** the overall accuracy of the simulation which remains based on the consecutive processing of both  $t^+$  and  $t^-$

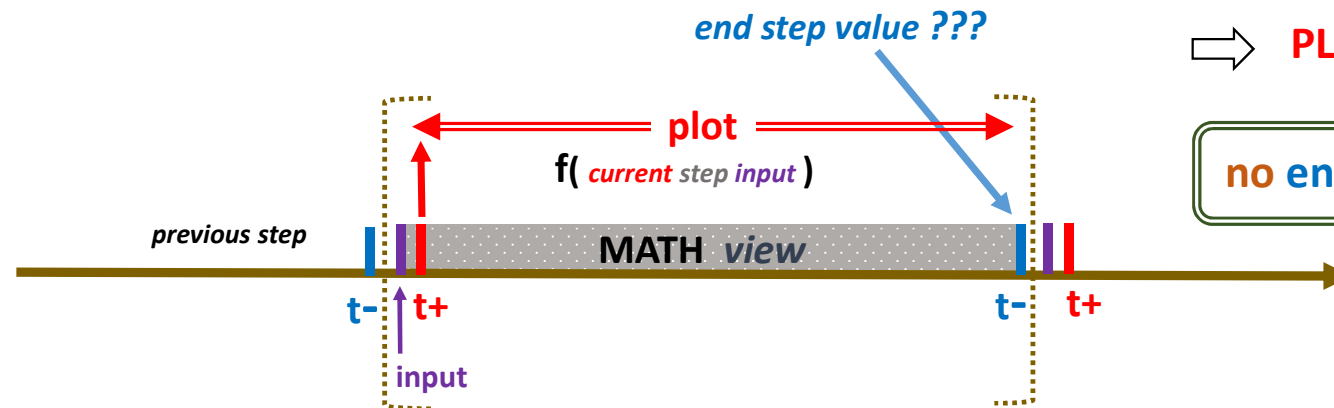
However, **this is only true** when the *entire simulated circuit* has been **edited** as a **single SARC schematic**

**ANALOG** view is required to simulate *assembly of blocks*





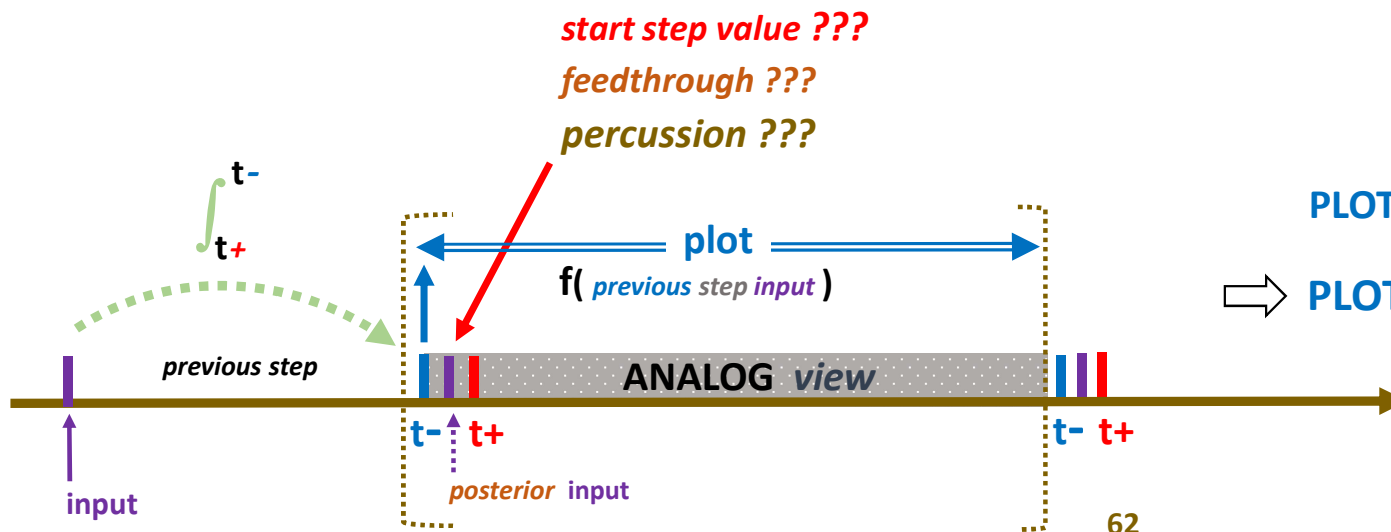
## SARC uncertainty



$$\text{PLOTS}(t) = f(\text{INPUTS}[t + \epsilon])$$

⇒ PLOTS are **concomitant** with INPUTS

no end value to enable assembly of blocks



$$\text{PLOTS}(t) = f(\text{INPUTS}[t - \epsilon])$$

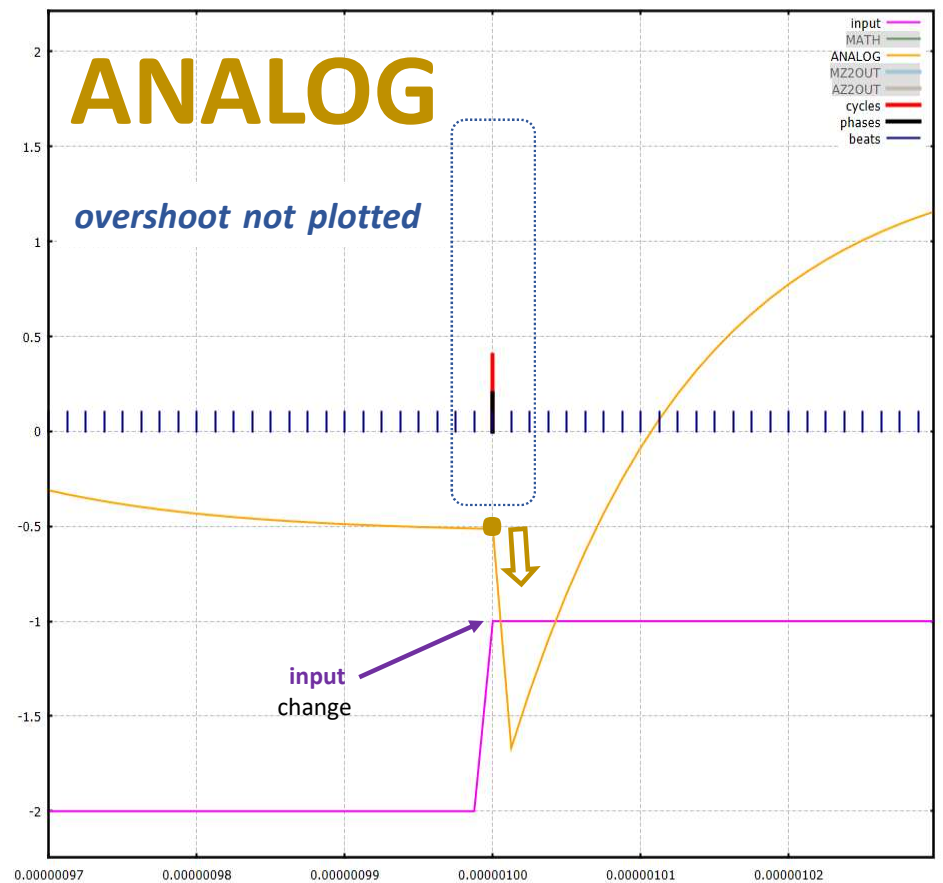
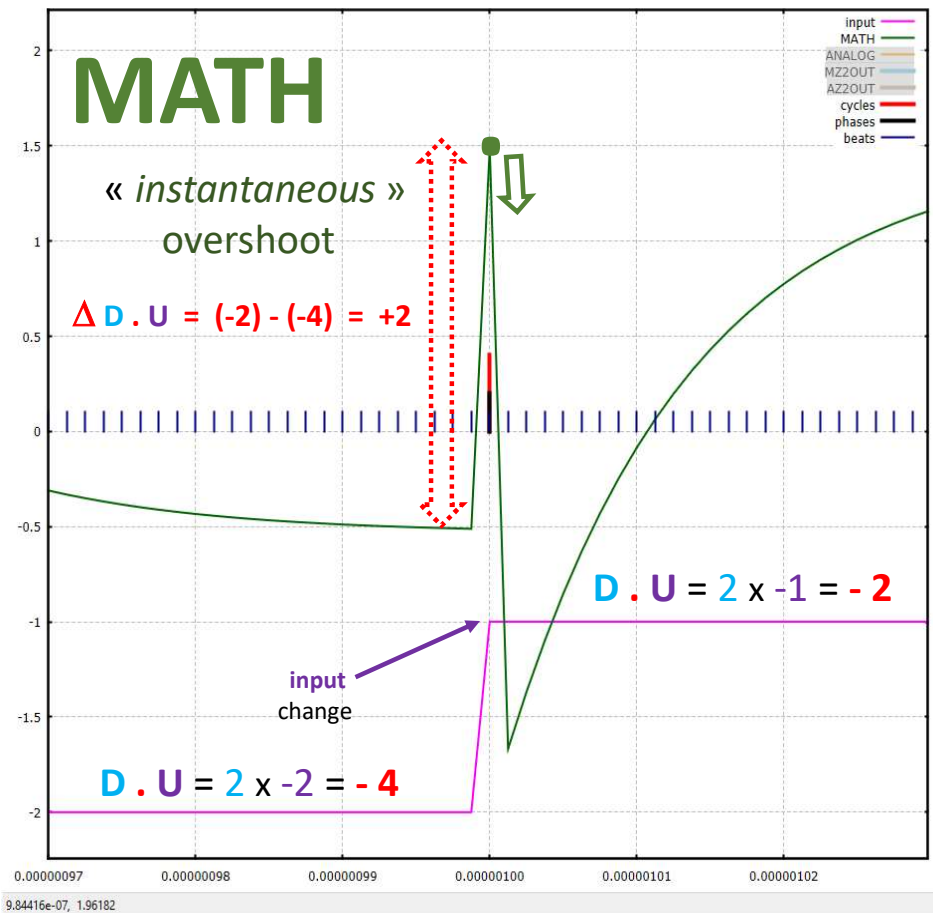
⇒ PLOTS are **postdated** versus INPUTS

## SARC uncertainty

$$Y = C \cdot X + D \cdot U$$

direct feedthrough path matrix  $D = \begin{bmatrix} 2 & 0 \end{bmatrix} \neq 0$

inputs vector  $U = \begin{bmatrix} -2 \\ 0 \end{bmatrix}$  followed by  $\begin{bmatrix} -1 \\ 0 \end{bmatrix}$

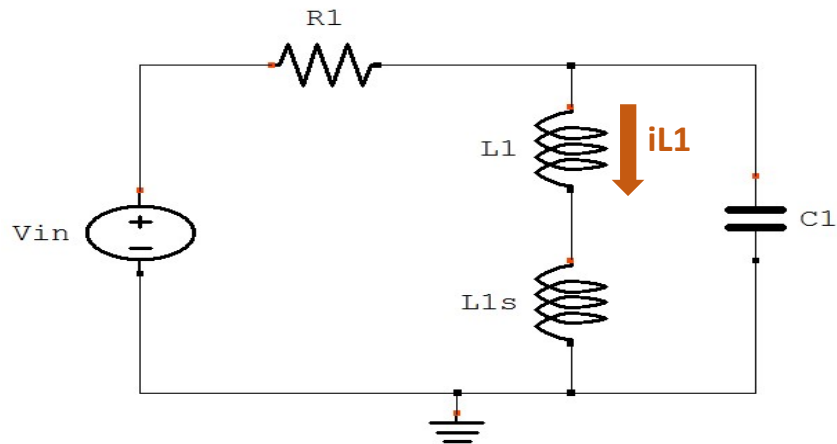


## SARC uncertainty

$$Y = C \cdot \underset{\text{state}}{X} + D \cdot U$$

*component value change*

could affect **C** or/and **D** ( and **X** if **LC** )

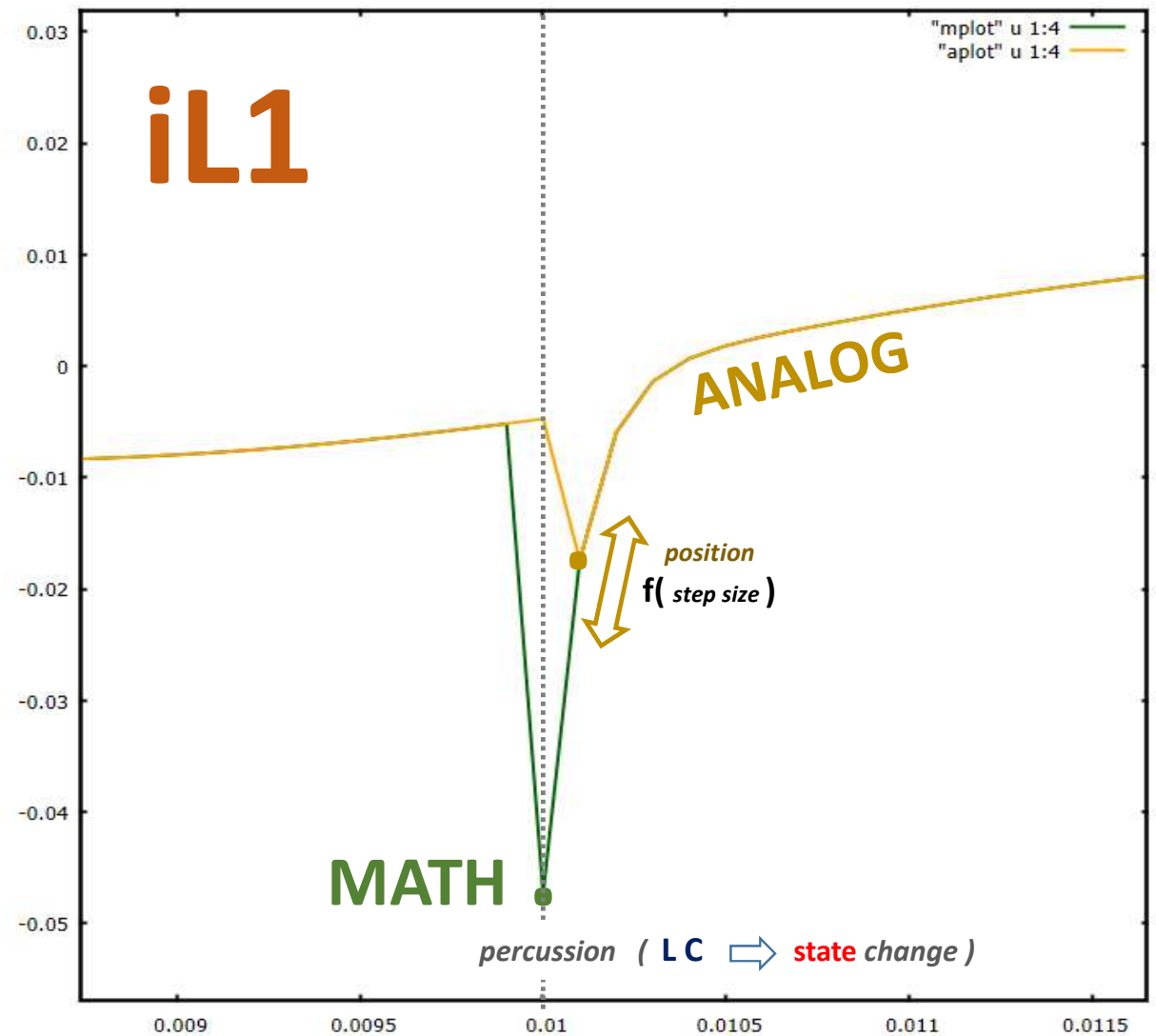


L1 = 90 mH  
L1s = 10 mH

at t = 0.01

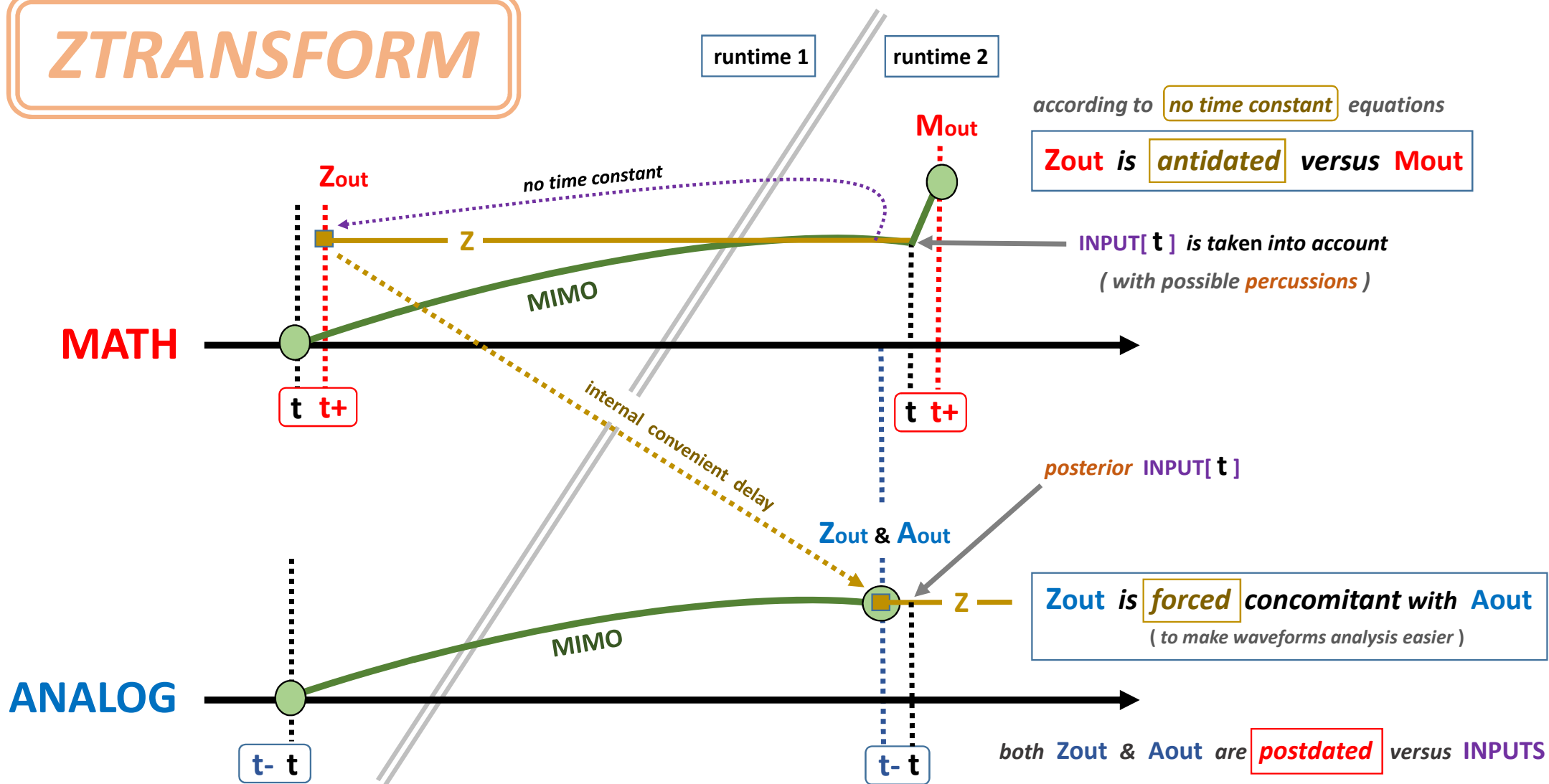
L1 = 6 mH  
L1s = 4 mH

64

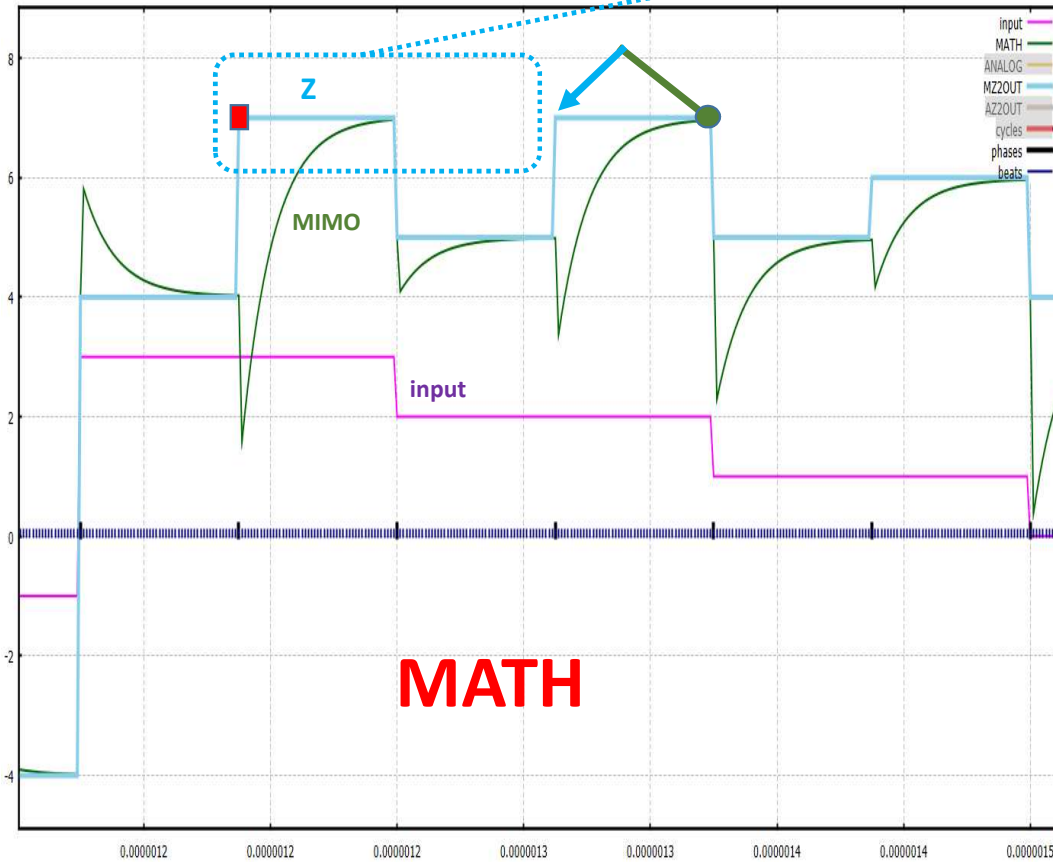




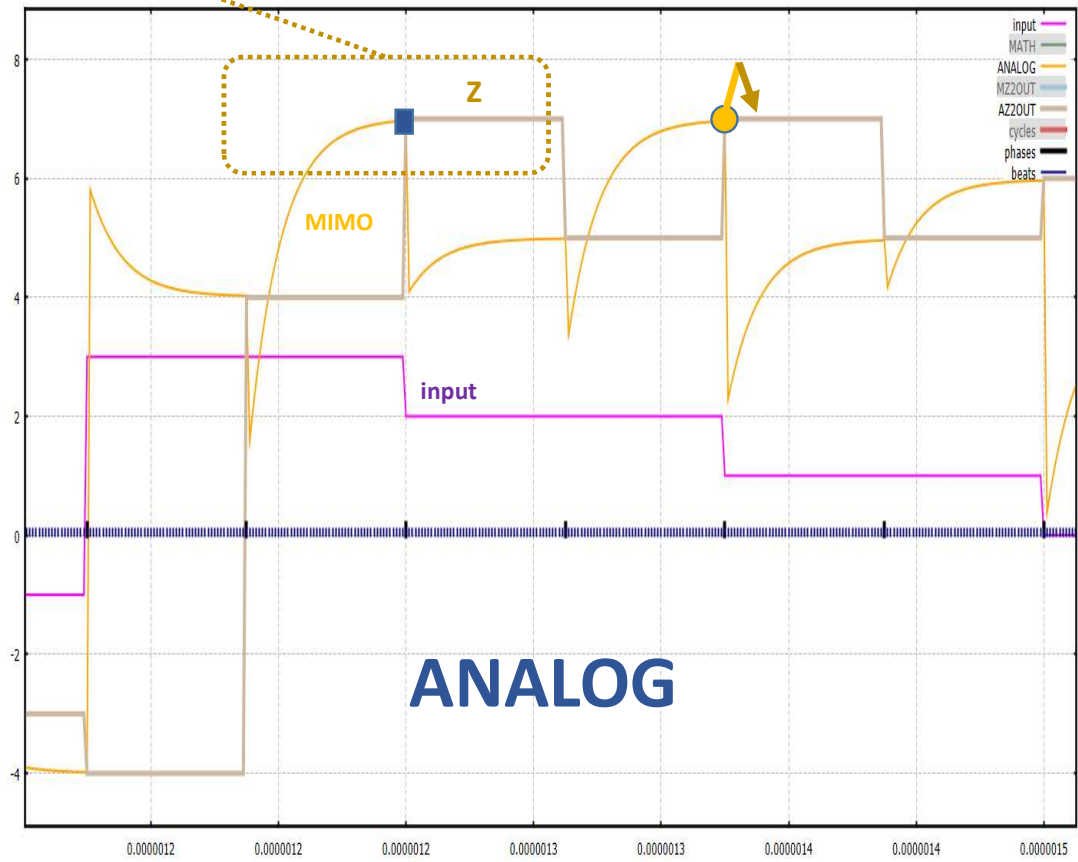
# ZTRANSFORM



**Z** earlier than **MIMO**



**Z** & **MIMO** concomitant

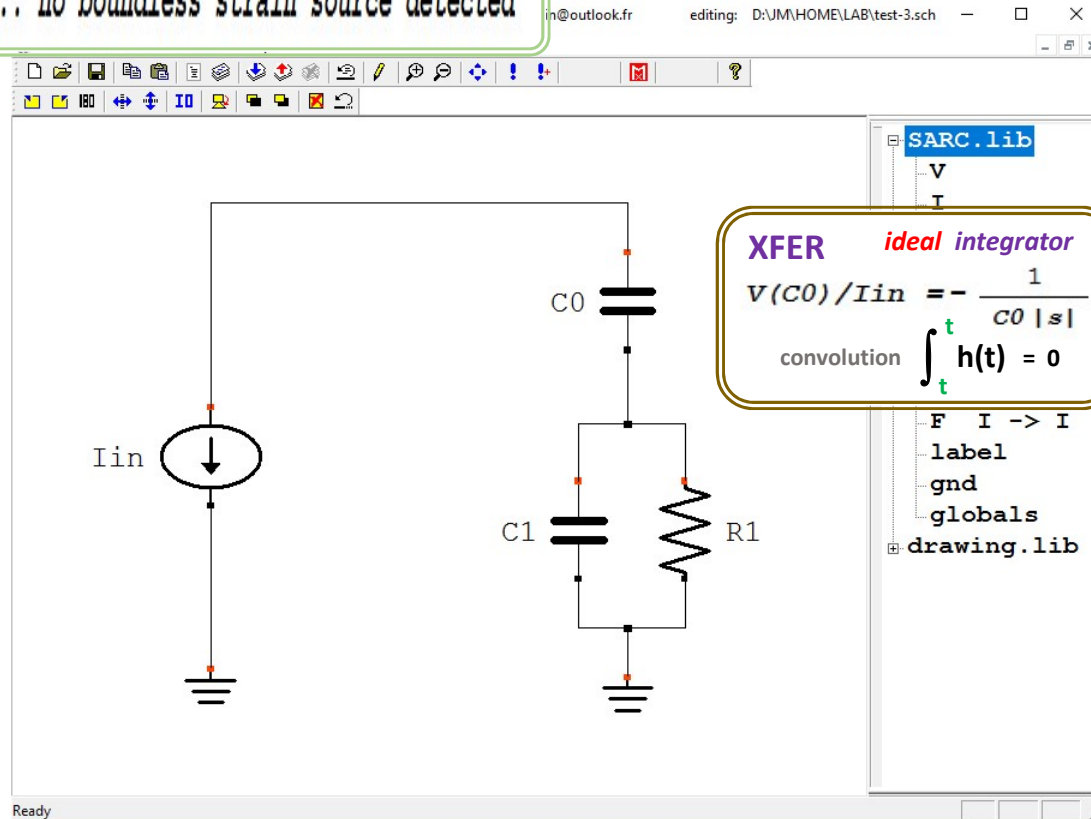


*runtime* **WARNINGS**

# WARNING

$$Y = 0$$

... no boundless strain source detected



conversion MIMO → XFER

1 warning  $V(C0)/I_{in} = 0$

2 proper  $V(C1)/I_{in} = -\frac{R1}{C1 R1 |s| + 1}$

MIMO simulation

### Warning : OUTPUT( V(C0) ) = 0

**please note :** the fact that  $V(C0)$  is **flagged** does not prevent  $V(C1)$  to be correct

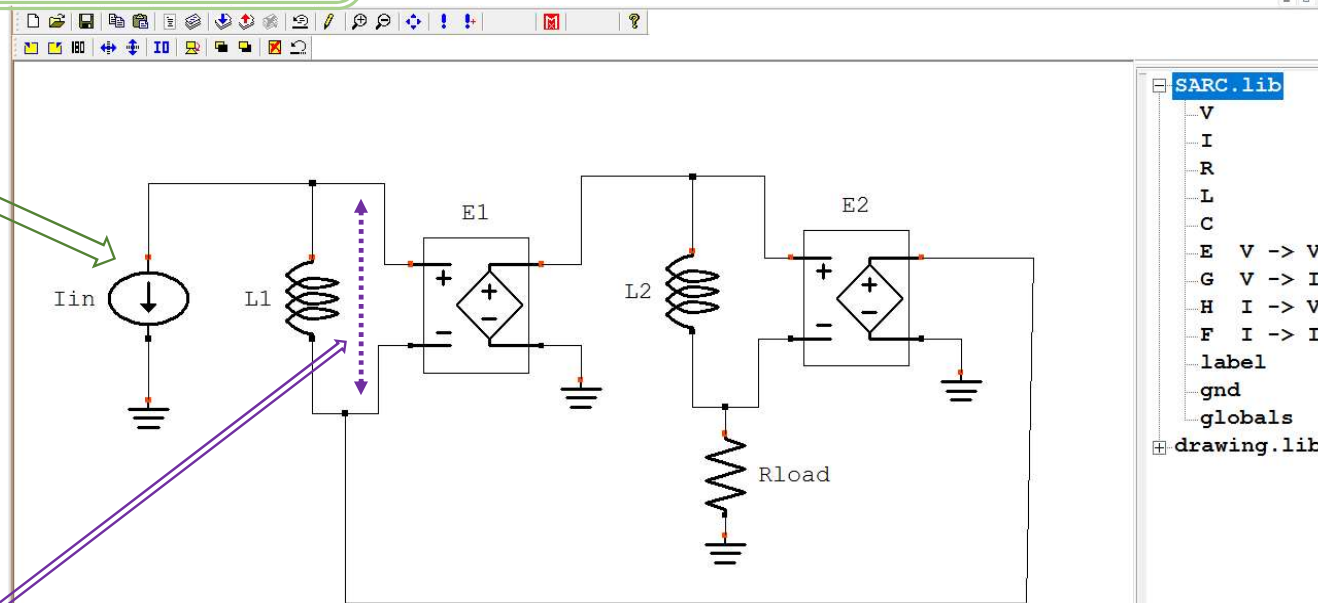
# WARNING

$$B = 0$$

### Warning : boundless strain sources [Iin]  
=> LC boundless strained [L1]

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boundless source



$$STATES = \begin{bmatrix} I(L2) \end{bmatrix}$$

A B C D

$$A = \begin{bmatrix} -\frac{Rload}{L2} \end{bmatrix}$$

$$B = \begin{bmatrix} 0 \end{bmatrix}$$

$$C = \begin{bmatrix} 1 \\ -E1 Rload \end{bmatrix}$$

$$D = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

XFER ideal derivative

improper  $cV(E1)/Iin = -L1 | s|$

MIMO simulation

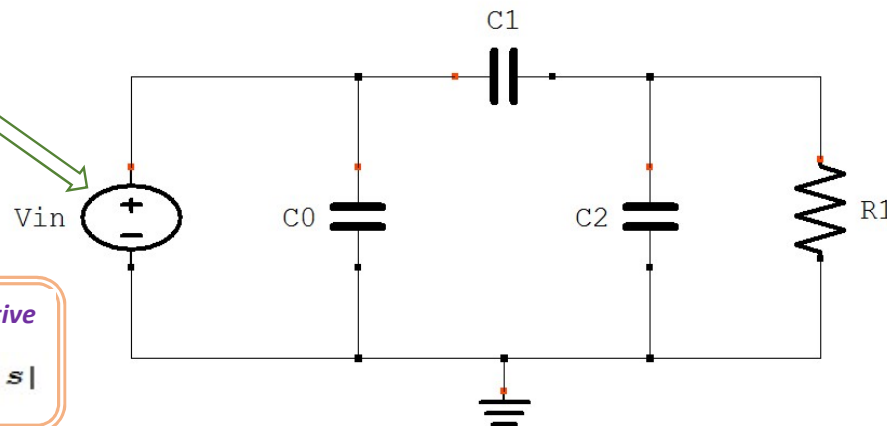
### Warning : OUTPUT( cV(E1) ) bad since B = 0  
### Warning : OUTPUT( I(Rload) ) bad since B = 0

# WARNING

$Y \neq 0$

### Warning : boundless strain sources [Vin]  
=> LC boundless strained [C0,C1,C2]

boundless source



XFER ideal derivative

improper  $I(C0)/Vin = C0 |s|$

MIMO simulation dubious output  $\neq 0$

### Warning : OUTPUT( I(C1) ) D[dubious states]

SARC.lib  
V  
I  
R  
L  
C  
E V -> V  
G V -> I  
H I -> V  
F I -> I  
label  
gnd  
globals  
drawing.lib

conversion MIMO  $\rightarrow$  XFER

biproper 
$$\frac{C1^2 |s|}{(C2 + C1)^2 R1 |s| + C2 + C1}$$

$\neq$

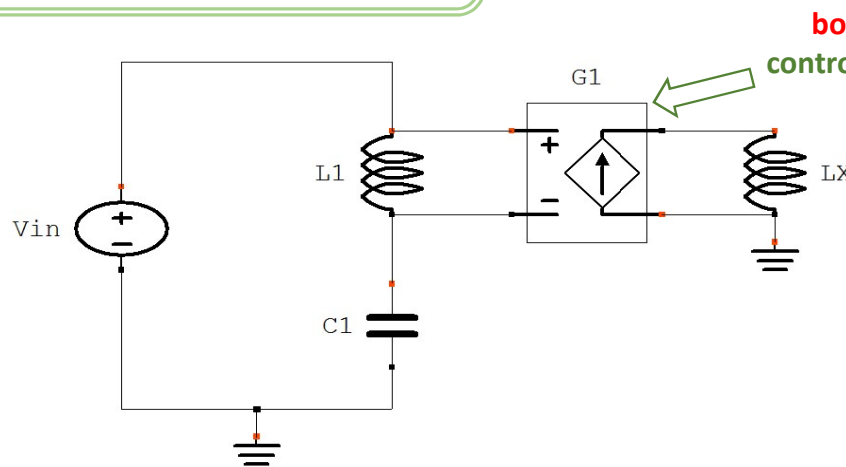
BUT corresponding XFER improper 
$$I(C1)/Vin = \frac{C1 C2 R1 |s|^2 + C1 |s|}{(C2 + C1) R1 |s| + 1}$$

# WARNING

$Y \neq 0$

### Warning : boundless strain sources [G1]

=> LC boundless strained [LX]



bipropor  $I(LX)/Vin = \frac{C1 G1 L1 |s|^2}{C1 L1 |s|^2 + 1}$

MIMO simulation dubious output  $\neq 0$

### Warning : OUTPUT( V(LX) ) C[dubious states]

conversion MIMO → XFER

proper  $-\frac{G1 LX |s|}{C1 L1 |s|^2 + 1}$

$\neq$

BUT corresponding XFER  $\text{improper } V(LX)/Vin = \frac{C1 G1 L1 LX |s|^3}{C1 L1 |s|^2 + 1}$

# BAD SCHEMATIC

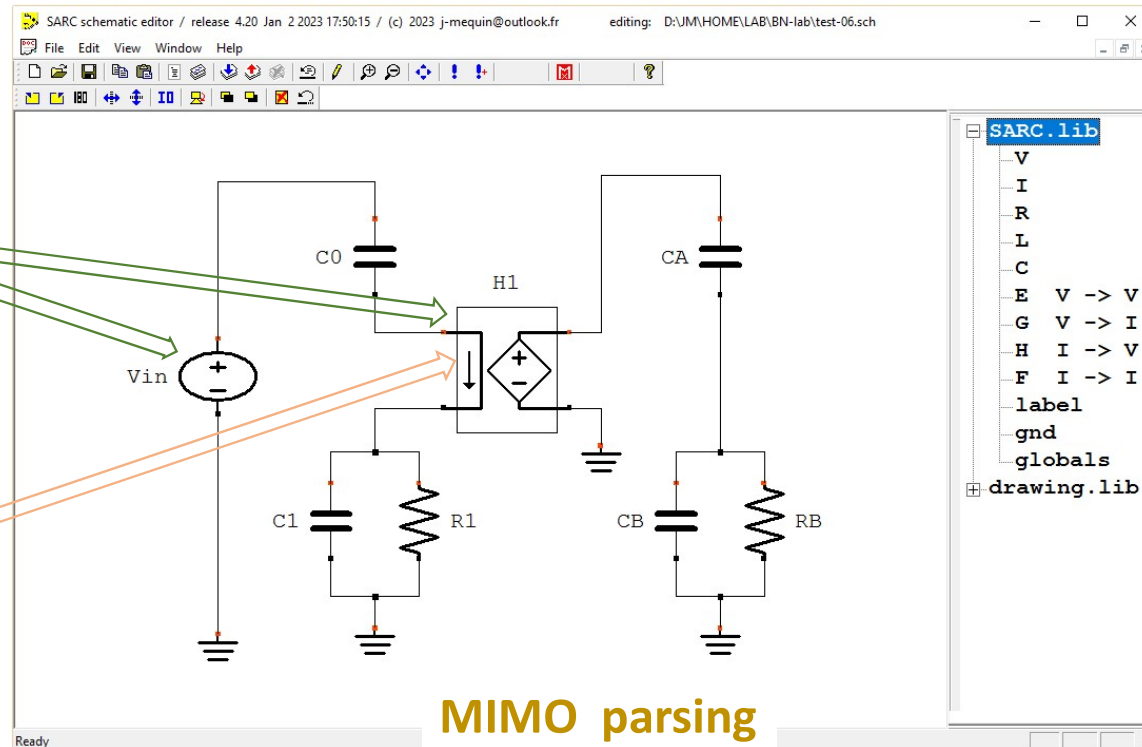
ABORT

### Warning : boundless strain sources [Vin,H1]  
=> LC boundless strained [C0,C1,CA,CB]

boundless sources

XFER

$$\text{improper } cI(H1)/Vin = \frac{C0 C1 R1 |s|^2 + C0 |s|}{(C1 + C0) R1 |s| + 1}$$



MIMO parsing

$$\left[ \begin{array}{c} U \quad X \\ Vin, CA, \frac{C0 C1 CB H1 |s|}{(C1 + C0) (CB + CA)} \end{array} \right], \left[ \begin{array}{c} U \quad X \\ Vin, CB, \frac{C0 C1 CA H1 |s|}{(C1 + C0) (CB + CA)} \end{array} \right]$$

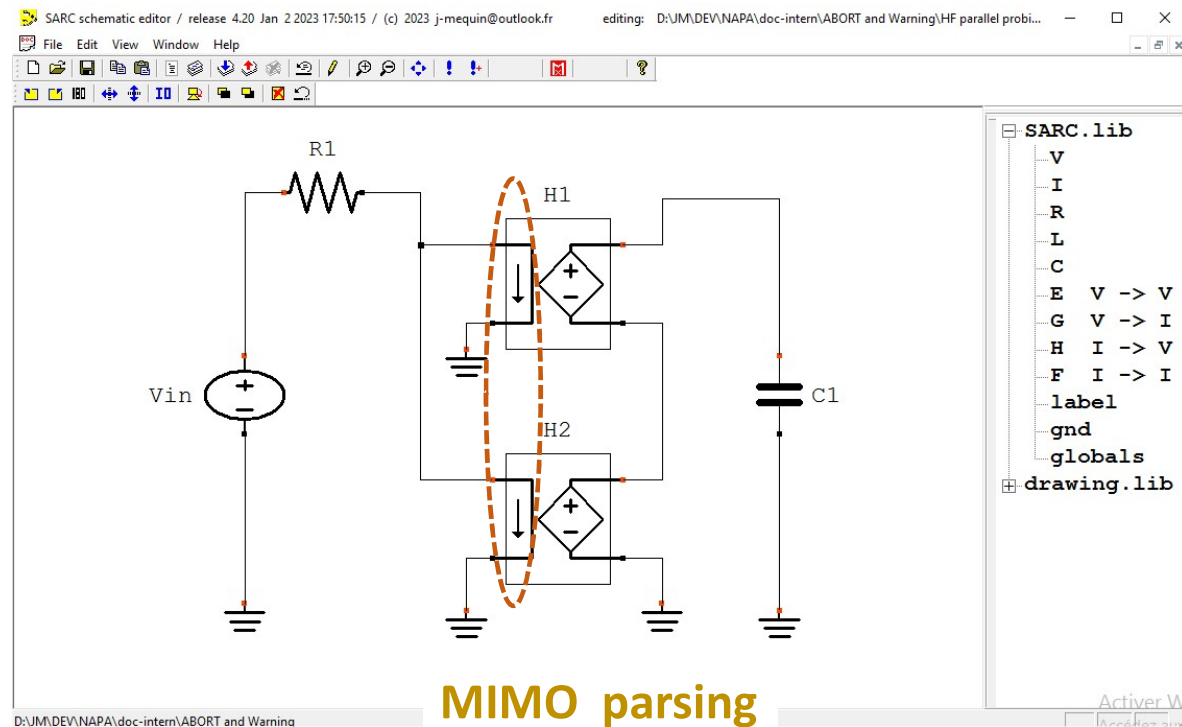
\*\*\* ERROR: improper STATES ["CA","CB"]



# BAD SCHEMATIC

ABORT

*schematic may look good but may not be simulable*



\*\*\* ERROR: parallel CURRENT probing for CONTROL side [{"H1","H2"}]